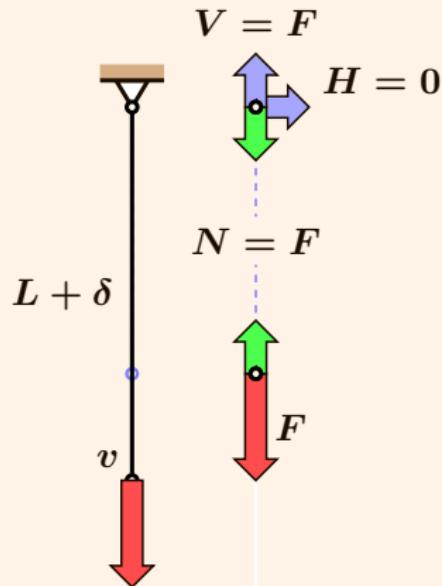


# **Sólido deformable: compatibilidad y equilibrio (3rd ed)**

Mariano Vázquez Espí

Madrid (España), 15 de marzo de 2017.

## Modelo 'cable'



# Modelo 'cable'

Equilibrio

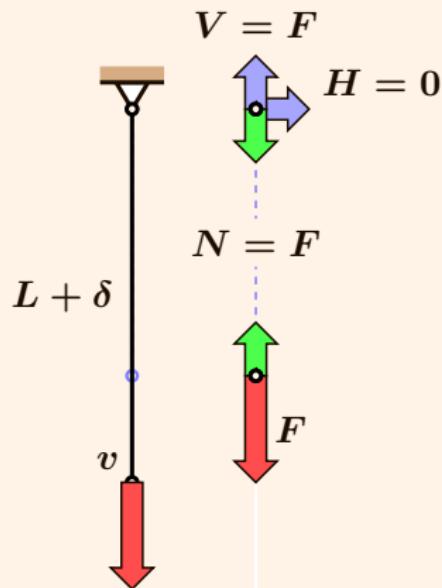
global

$$F = V \quad H = 0$$

interno

$$N = \sigma A$$

$$N = F$$



# Modelo 'cable'

Equilibrio

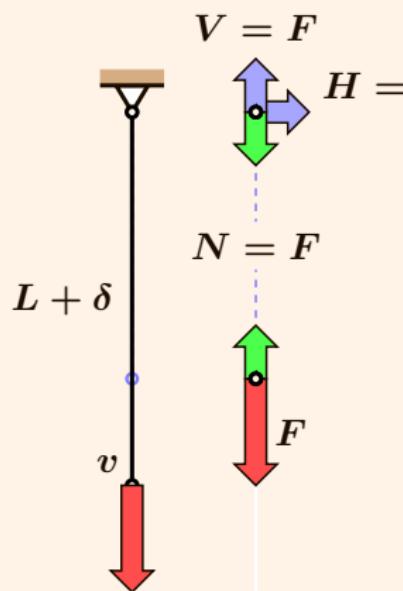
global

$$F = V \quad H = 0$$

interno

$$N = \sigma A$$

$$N = F$$



Compatibilidad

$$\delta = \varepsilon L$$

$$\delta = v$$

# Modelo 'cable'

## Equilibrio

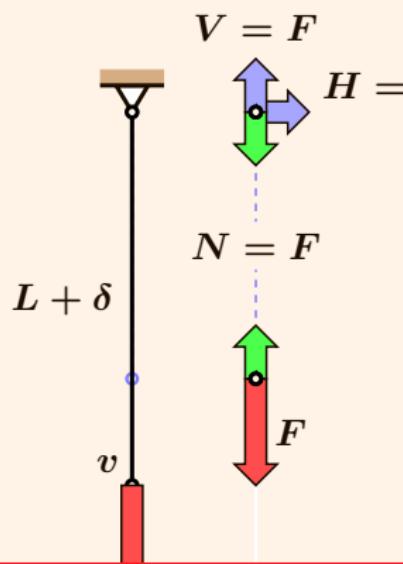
global

$$F = V \quad H = 0$$

interno

$$N = \sigma A$$

$$N = F$$



## Compatibilidad

$$\delta = \varepsilon L$$

$$\delta = v$$

## Material

$$\sigma = \begin{cases} \varepsilon E & \text{si } 0 \leq \varepsilon \leq \varepsilon_e \\ f_u & \text{si } \varepsilon_e \leq \varepsilon \leq \varepsilon_u \\ 0 & \text{en cualquier otro caso} \end{cases}$$

# Modelo 'cable'

## Equilibrio

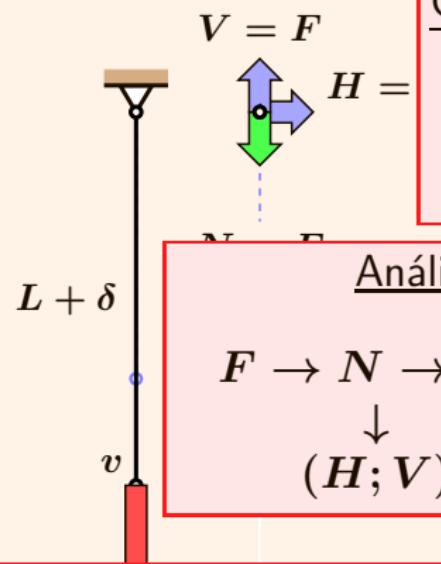
global

$$F = V \quad H = 0$$

interno

$$N = \sigma A$$

$$N = F$$



## Compatibilidad

$$\delta = \varepsilon L$$

$$\delta = v$$

## Análisis isostático

$$F \rightarrow N \rightarrow \sigma \rightarrow \varepsilon \rightarrow \delta \rightarrow v$$

↓

$(H; V)$

## Material

$$\sigma = \begin{cases} \varepsilon E & \text{si } 0 \leq \varepsilon \leq \varepsilon_e \\ f_u & \text{si } \varepsilon_e \leq \varepsilon \leq \varepsilon_u \\ 0 & \text{en cualquier otro caso} \end{cases}$$

## Ecuaciones de equilibrio

---

Son las relaciones entre las fuerzas interiores de los sólidos deformables y las acciones sobre la estructura bajo la condición de equilibrio estático.

En su forma más básica expresan las resultantes  $H, V, M, \dots$  de los esfuerzos  $N_1, N_2, N_3, \dots$ . Cada condición de equilibrio ( $H, V, M, \dots$ ) resulta en una ecuación.

En estructuras sometidas a requisitos de rigidez con distorsiones tolerables muy pequeñas, se pueden escribir a partir de la geometría indeformada de la estructura sin perdida significativa de precisión, resultando en ecuaciones lineales.

## Ecuaciones de compatibilidad

---

Son las relaciones entre movimientos de puntos o sólidos indeformables y la deformación de los sólidos deformables. Expresan la coherencia topológica y geométrica entre las distintas partes de una estructura y son validas siempre que la estructura no se rompa, sin importar el estado elástico o plástico de sus partes.

En su forma más básica relacionan movimientos  $u, v, \theta, \dots$  con alargamientos  $\delta_1, \delta_2, \dots$

En estructuras sometidas a requisitos de rigidez con distorsiones tolerables muy pequeñas, se pueden escribir como relaciones lineales de forma casi exacta (hipótesis de pequeñas deformaciones).

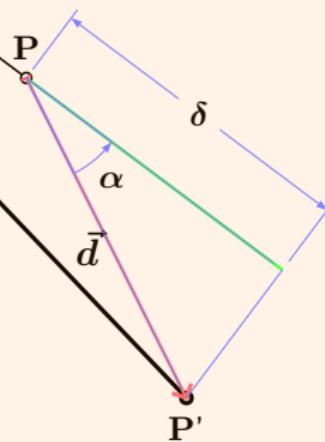
**Se deducen de dibujos para cada  $u, v, \theta, \dots$**

# Ecuaciones de compatibilidad



Desplazamiento genérico  $\vec{d}$  de P

$$\delta = d \cos \alpha$$

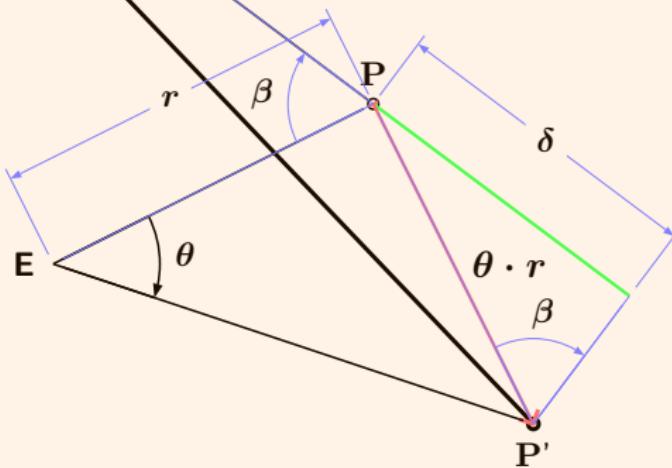


# Ecuaciones de compatibilidad



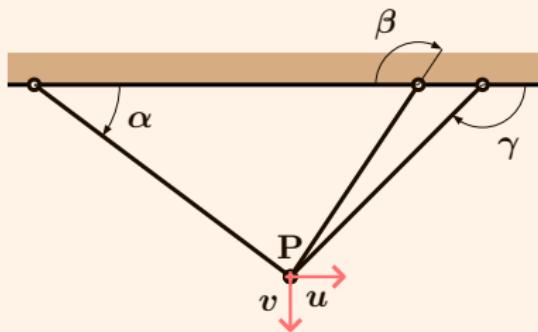
Giro genérico  $\vec{\theta}$  con centro en **E**

$$\delta = (\theta \cdot r) \sin \beta$$

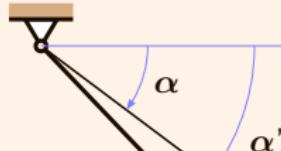


# Ecuaciones de compatibilidad

Deformaciones:  $\delta_a; \delta_b; \delta_c$ . Movimientos:  $u; v$

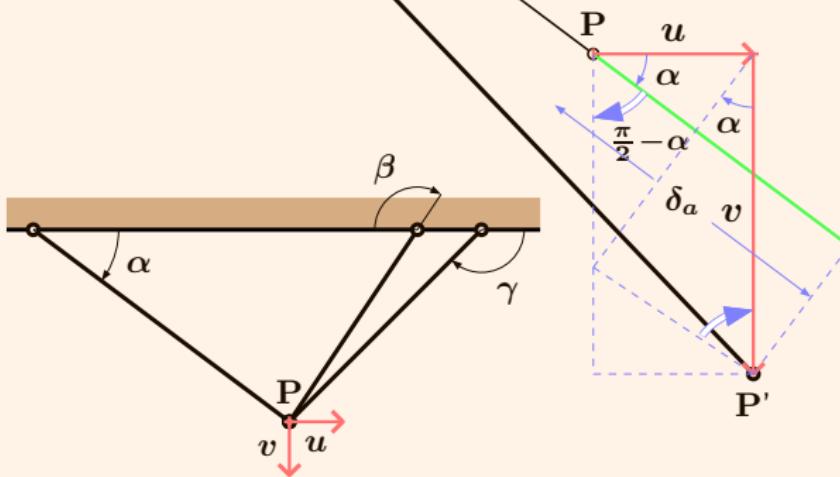


# Ecuaciones de compatibilidad

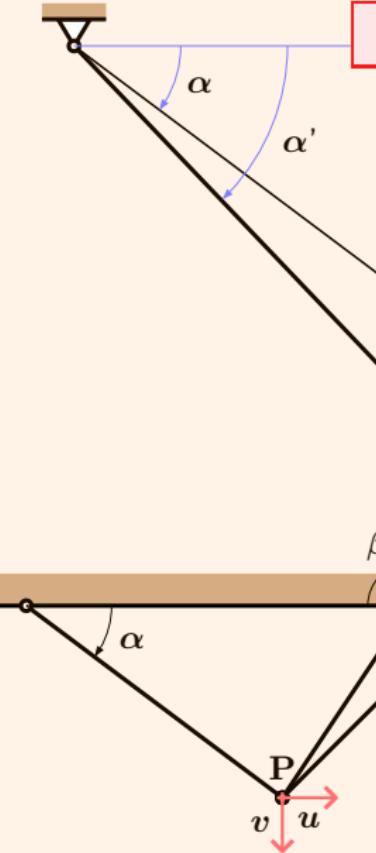


Deformaciones:  $\delta_a; \delta_b; \delta_c$ . Movimientos:  $u; v$

$$\begin{aligned}\delta_a &= u \cos \alpha + v \sin \alpha \\ \delta_a(u) &= u \cos \alpha \\ \delta_a(v) &= v \cos \left( \frac{\pi}{2} - \alpha \right)\end{aligned}$$

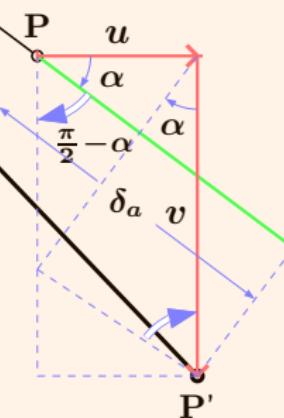


# Ecuaciones de compatibilidad

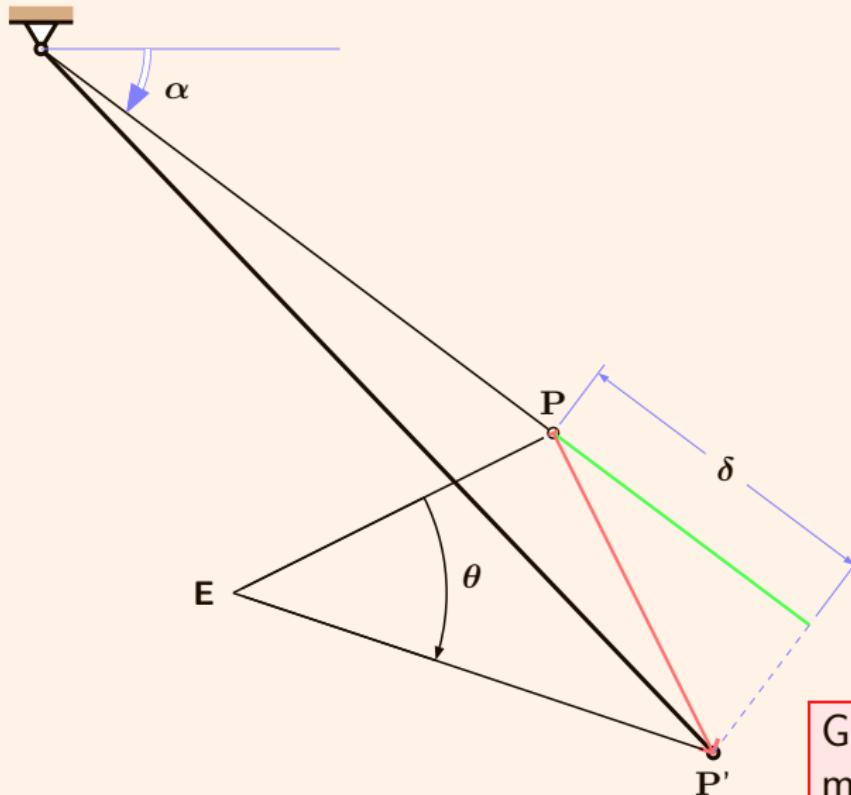


Deformaciones:  $\delta_a; \delta_b; \delta_c$ . Movimientos:  $u; v$

$$\begin{aligned}\delta_a &= u \cos \alpha + v \sin \alpha \\ \delta_b &= u \cos \beta + v \sin \beta \\ \delta_c &= u \cos \gamma + v \sin \gamma\end{aligned}$$



# Ecuaciones de compatibilidad

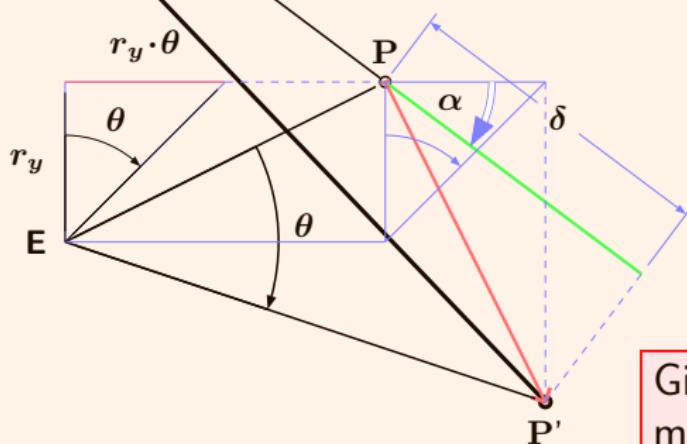


Giro,  
movimientos  $u, v$   
y alargamientos

# Ecuaciones de compatibilidad

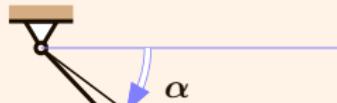


$$u = \theta \cdot r_y$$
$$\delta(r_y) = (\theta \cdot r_y) \cos \alpha$$

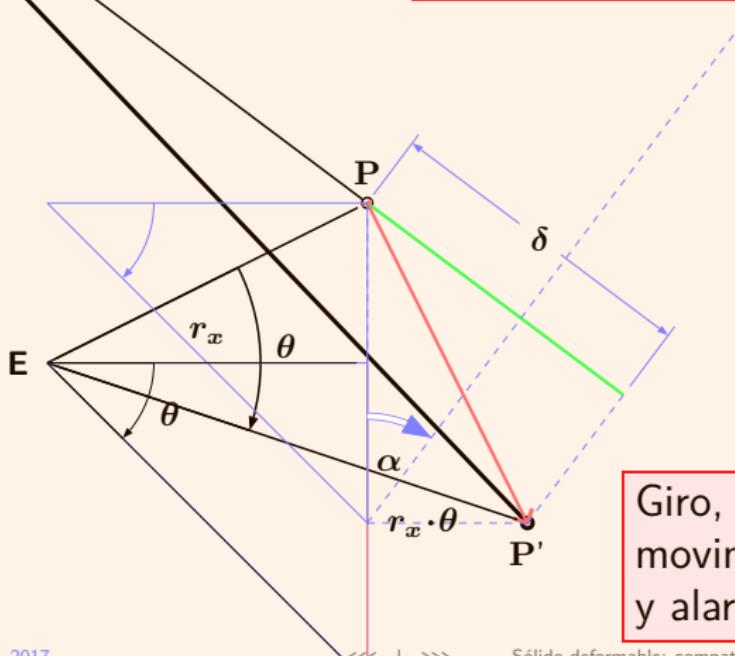


Giro,  
movimientos  $u, v$   
y alargamientos

# Ecuaciones de compatibilidad

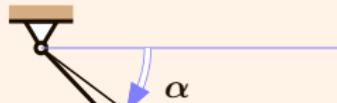


$$u = \theta \cdot r_y$$
$$\delta(r_y) = (\theta \cdot r_y) \cos \alpha$$
$$v = \theta \cdot r_x$$
$$\delta(r_x) = (\theta \cdot r_x) \sin \alpha$$

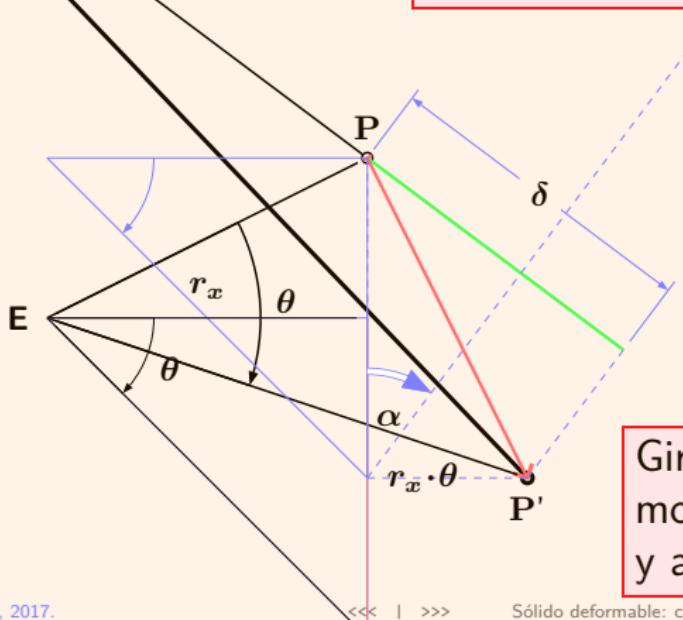


Giro,  
movimientos  $u, v$   
y alargamientos

# Ecuaciones de compatibilidad



$$\begin{aligned} u &= \theta \cdot r_y \\ \delta(r_y) &= (\theta \cdot r_y) \cos \alpha \\ v &= \theta \cdot r_x \\ \delta(r_x) &= (\theta \cdot r_x) \sin \alpha \\ \delta &= \theta \cdot (r_y \cos \alpha + r_x \sin \alpha) \end{aligned}$$



Giro,  
movimientos  $u, v$   
y alargamientos

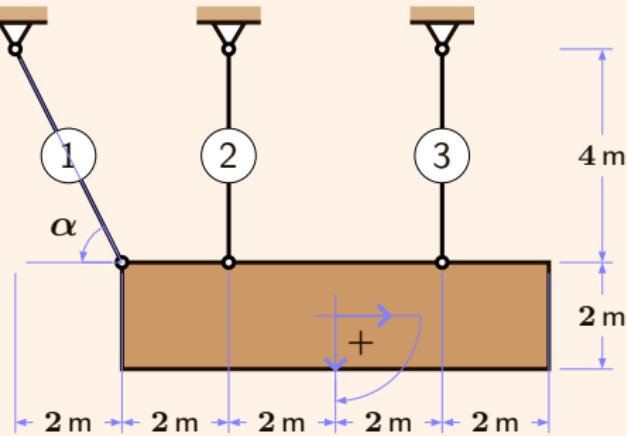
## Algunos ejemplos

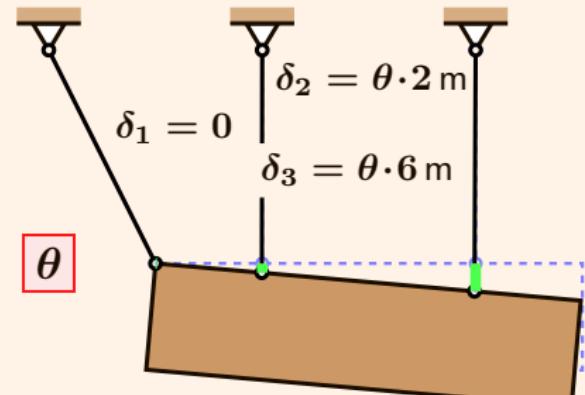
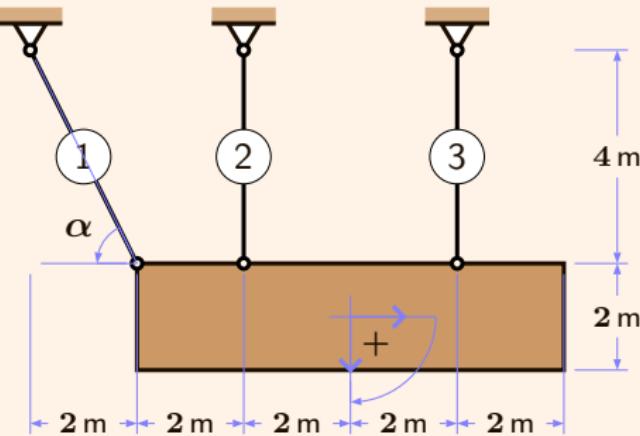
En los ejemplos siguientes tres cables sostienen una piedra con distintas geometrías y sustentación.

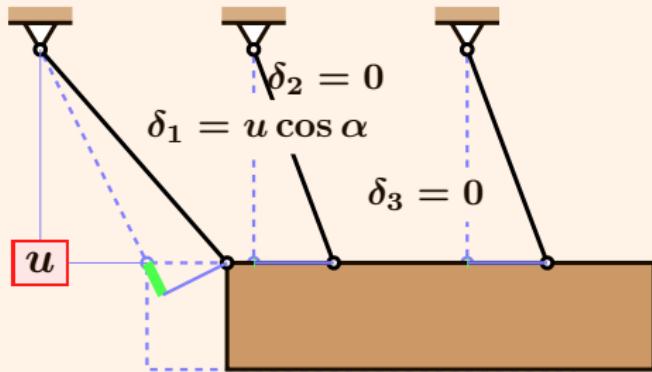
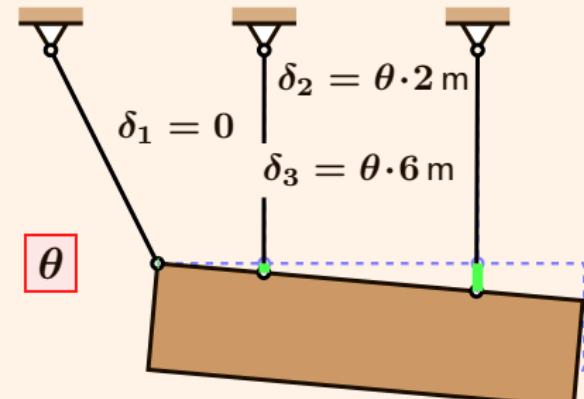
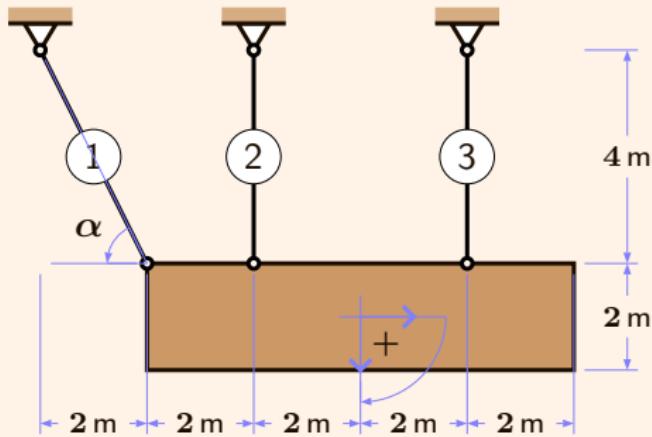
La piedra en principio tiene tres grados de libertad,  $u, v, \theta$ . Para cada uno de ellos se realiza un dibujo, suponiendo valores nulos para los otros dos. Y en cada dibujo, o bien se deduce que el grado de libertad es incompatible con la sustentación, o bien se deducen su relación con los alargamientos de los cables.

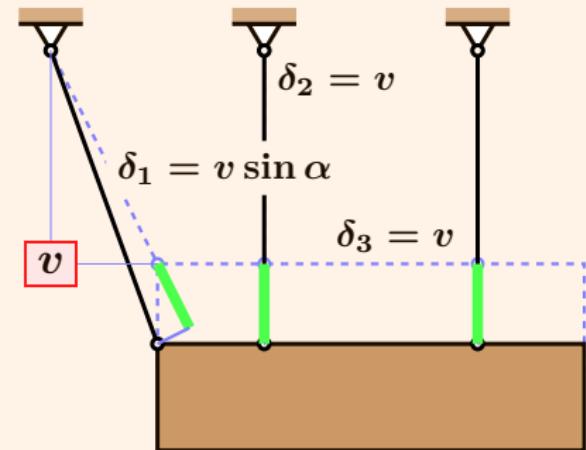
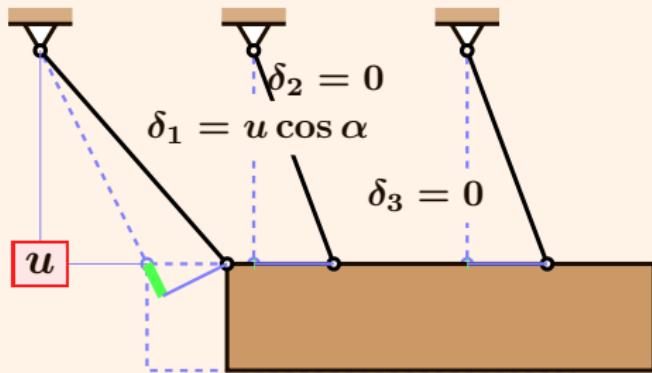
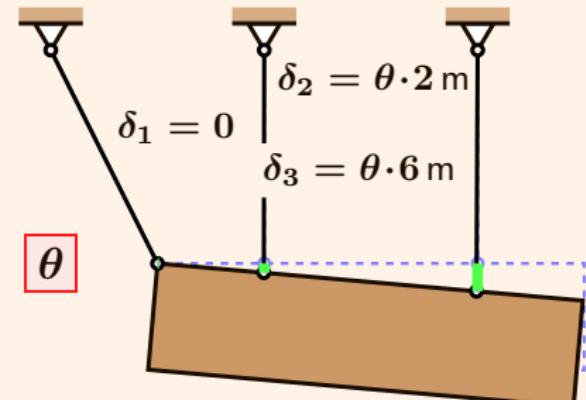
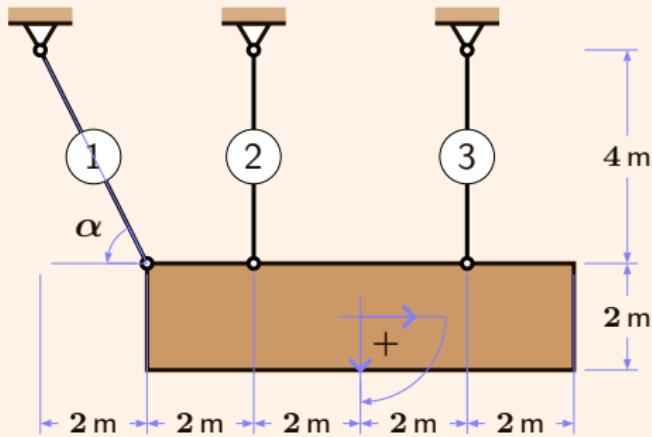
Las ecuaciones de compatibilidad, finalmente, se forman sumando las contribuciones de cada grado a cada alargamiento.

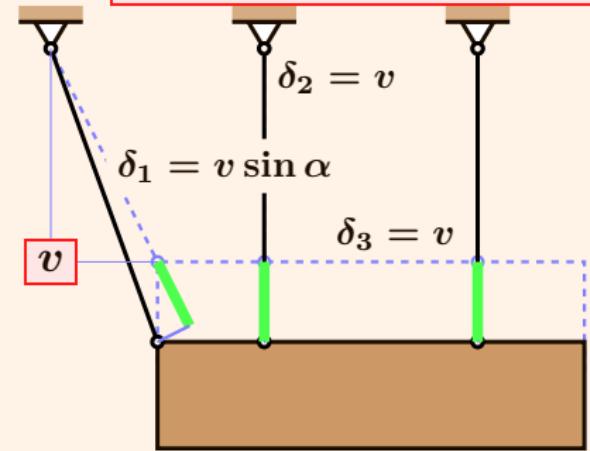
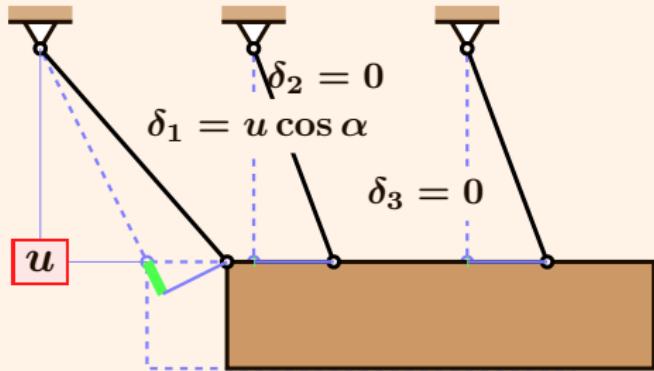
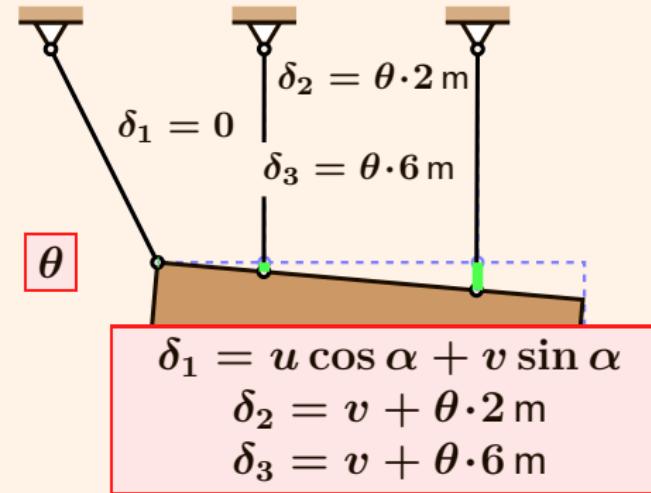
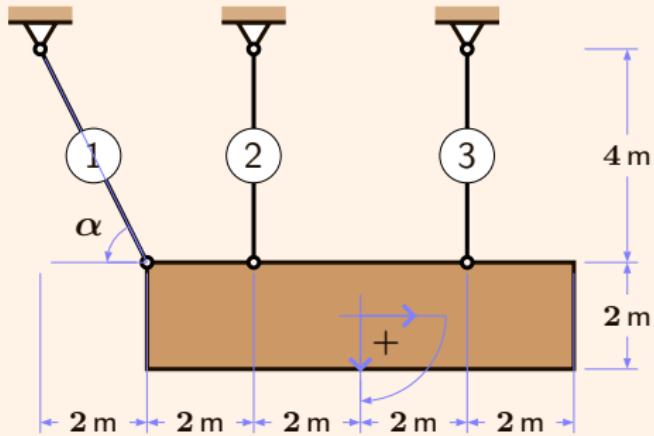
Las ecuaciones de equilibrio son las “traspuestas” de las anteriores, aunque se pueden deducir directamente.

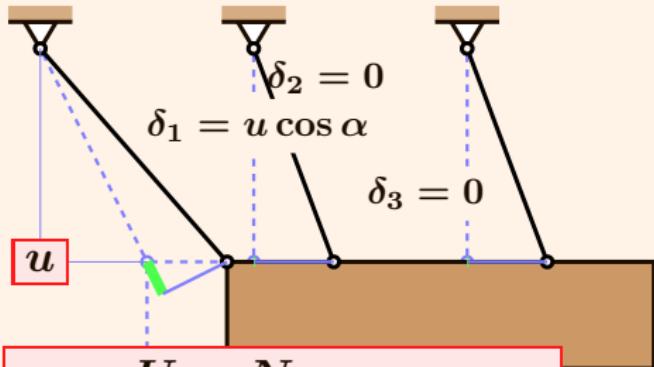
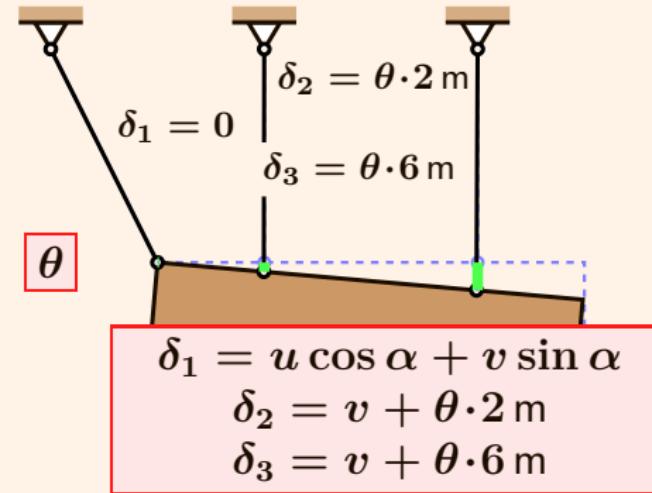
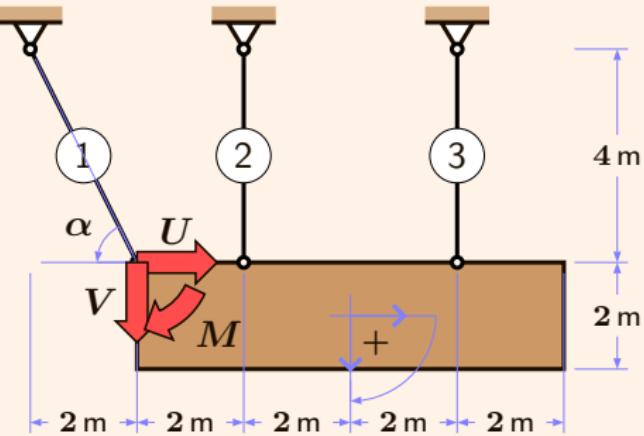








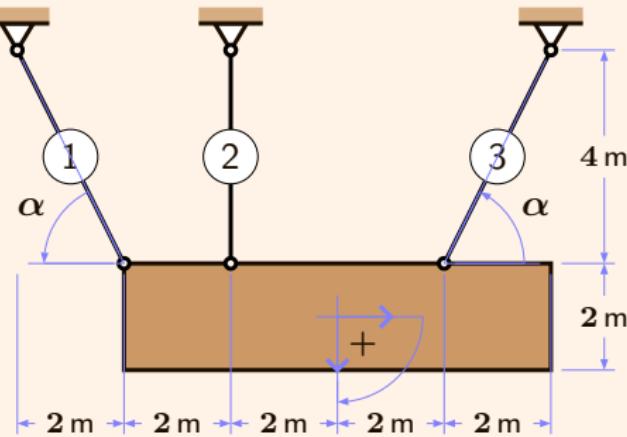


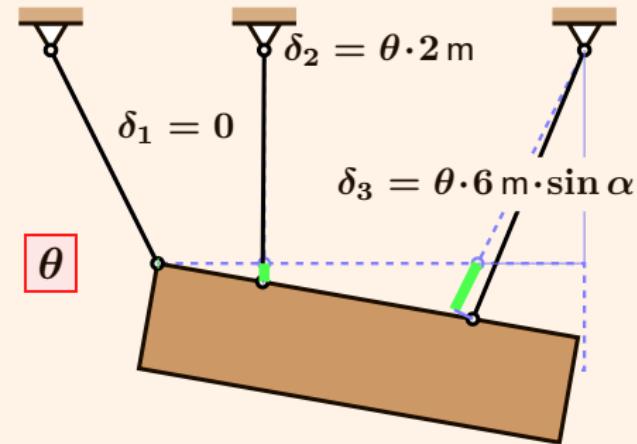
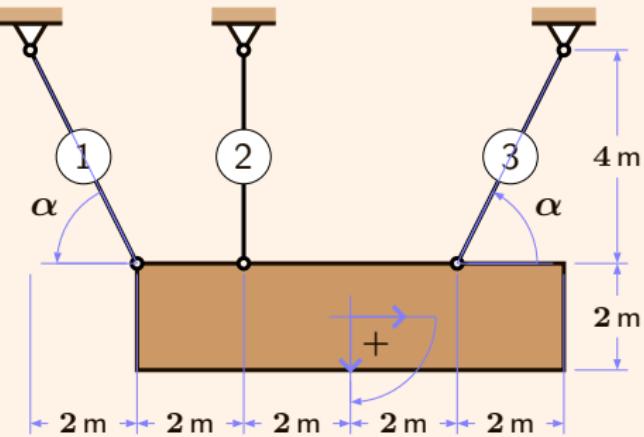


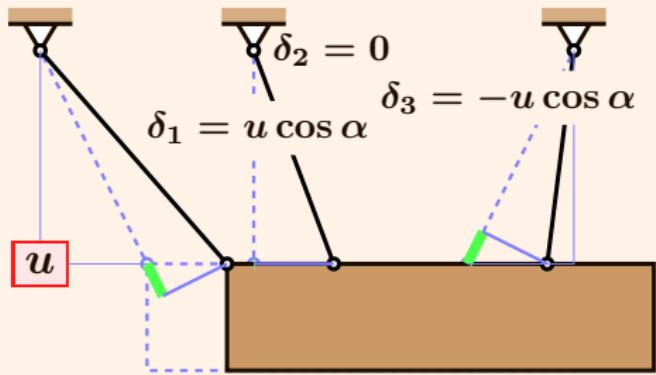
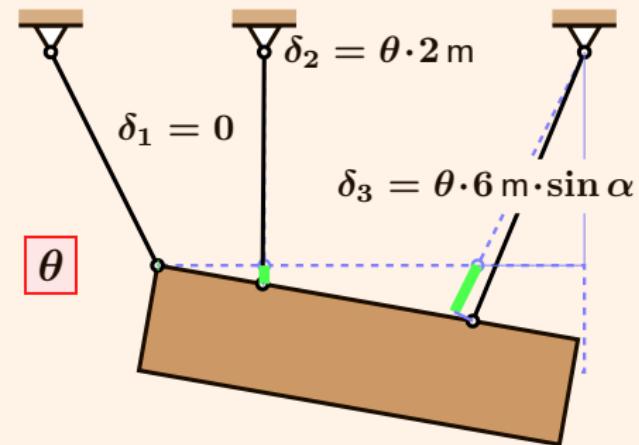
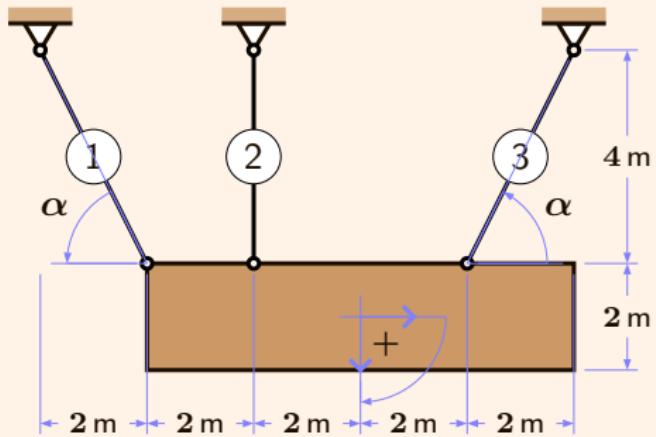
$U = N_1 \cos \alpha$   
 $V = N_1 \sin \alpha + N_2 + N_3$   
 $M = N_2 \cdot 2 \text{ m} + N_3 \cdot 6 \text{ m}$

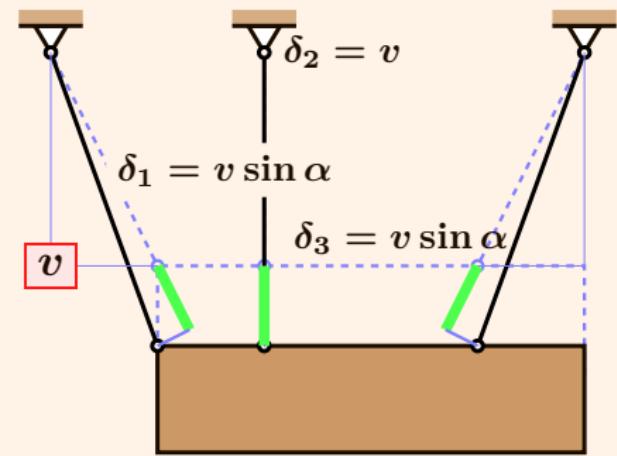
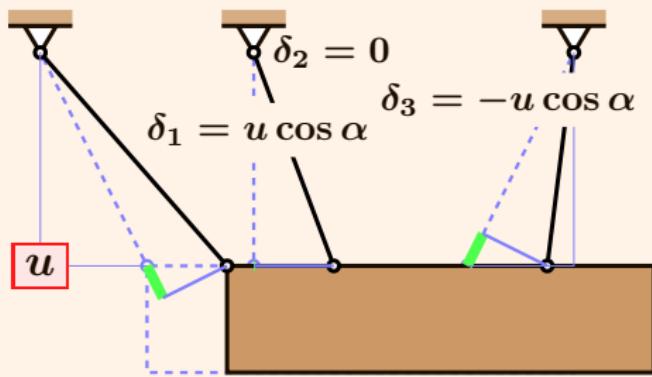
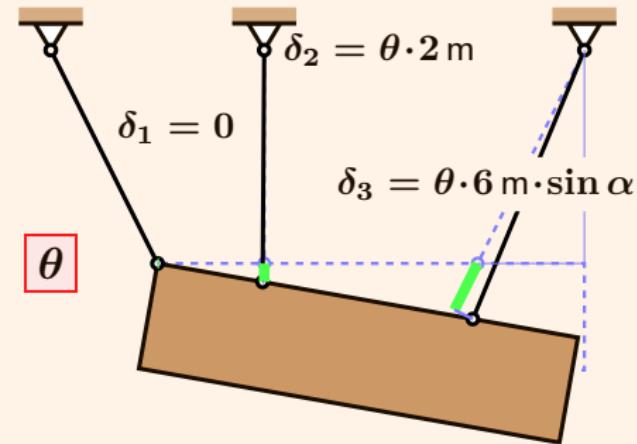
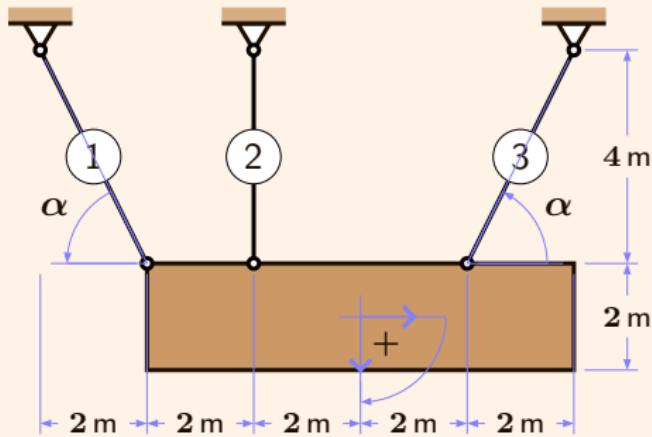
Copyright © Vázquez Espí, 2017.

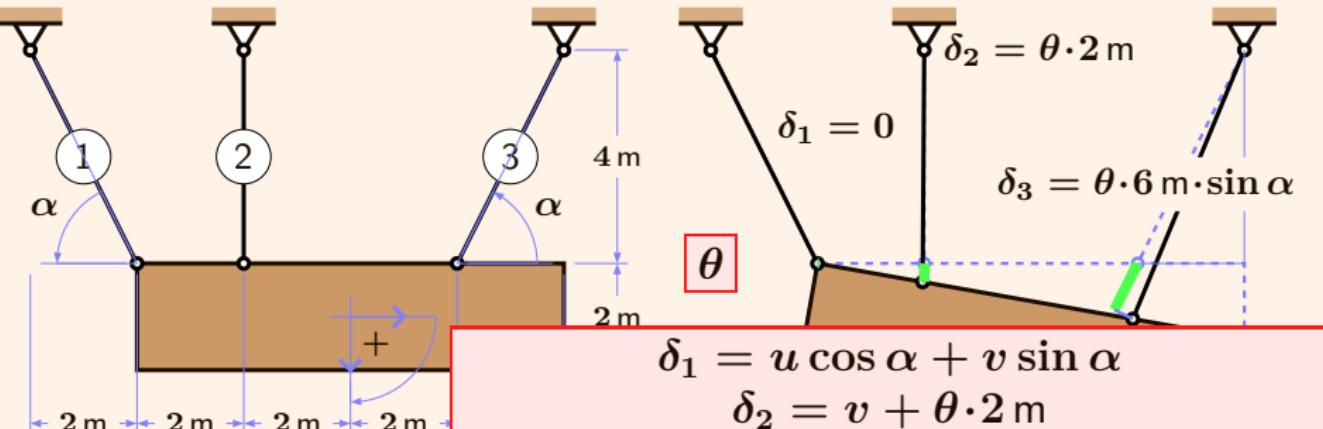
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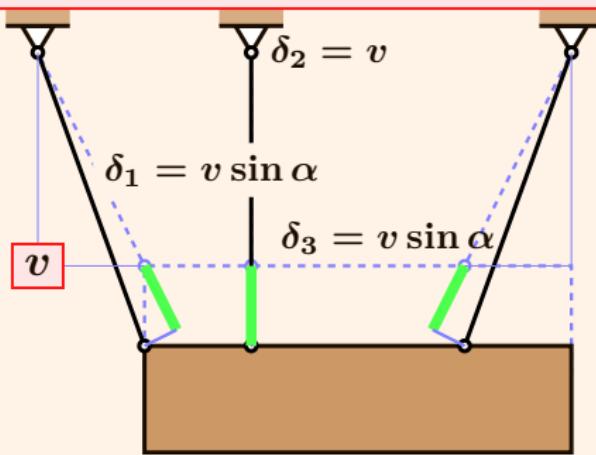
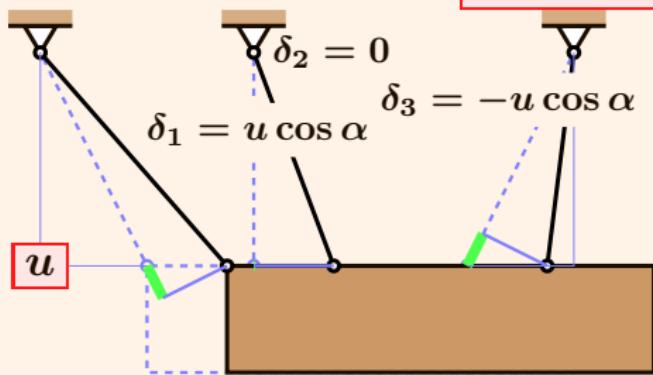


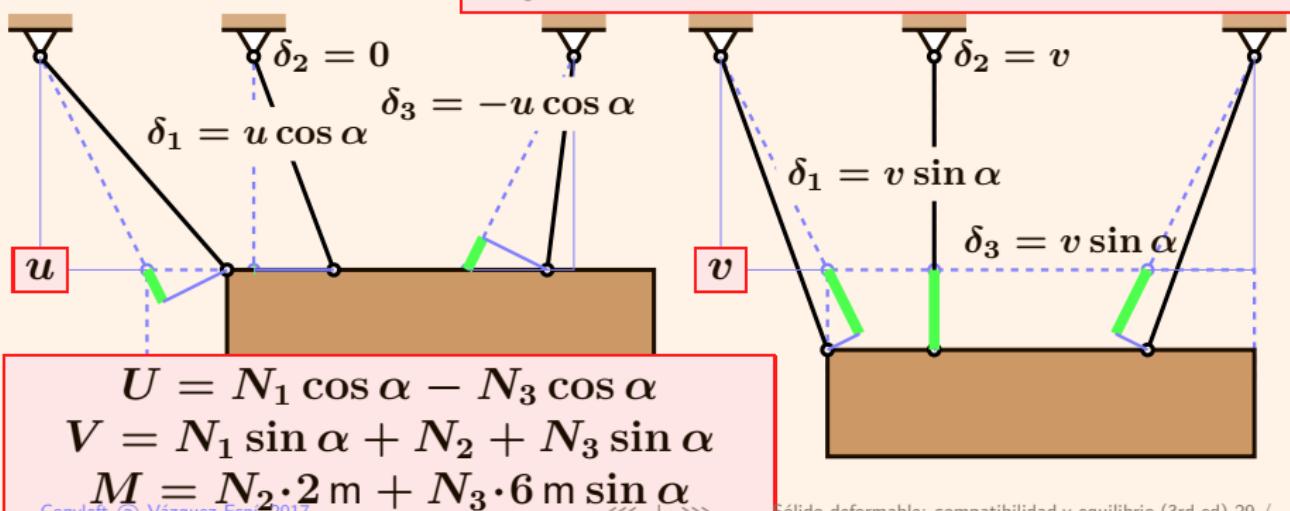
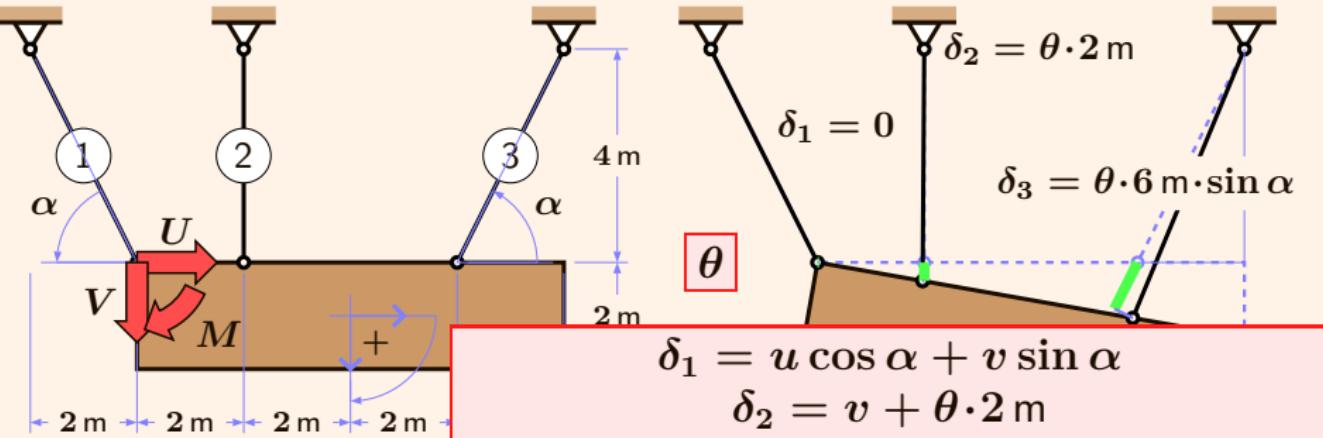
$\theta$

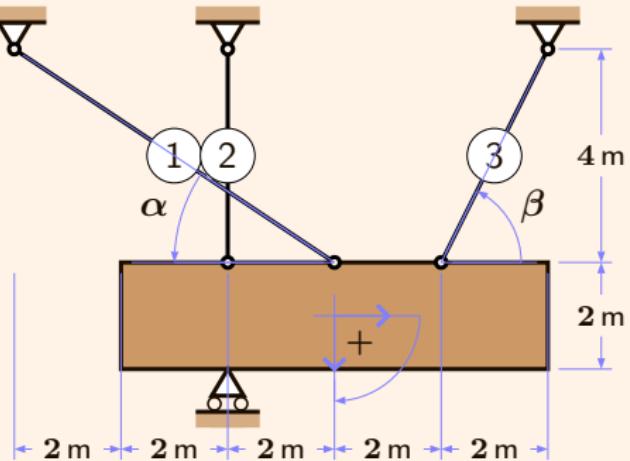
$$\delta_1 = u \cos \alpha + v \sin \alpha$$

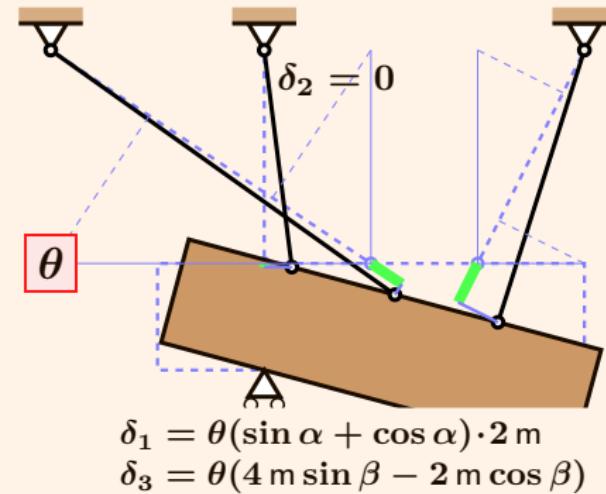
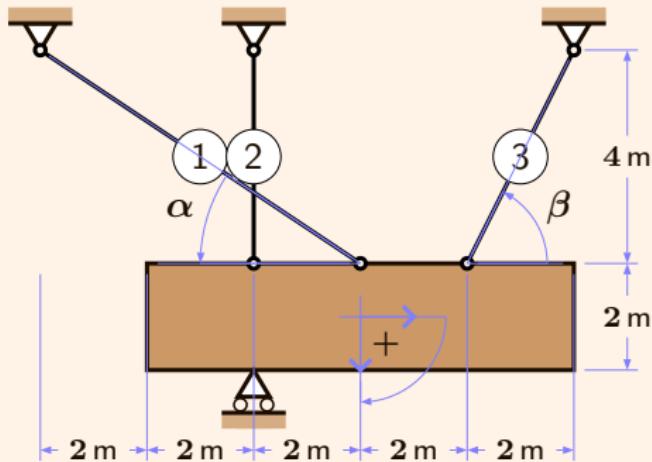
$$\delta_2 = v + \theta \cdot 2 \text{ m}$$

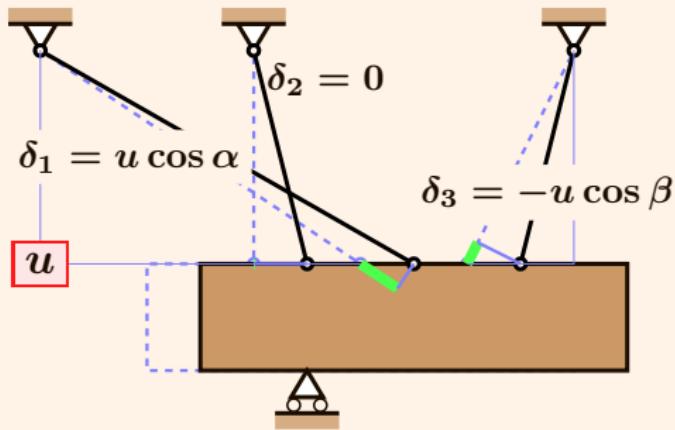
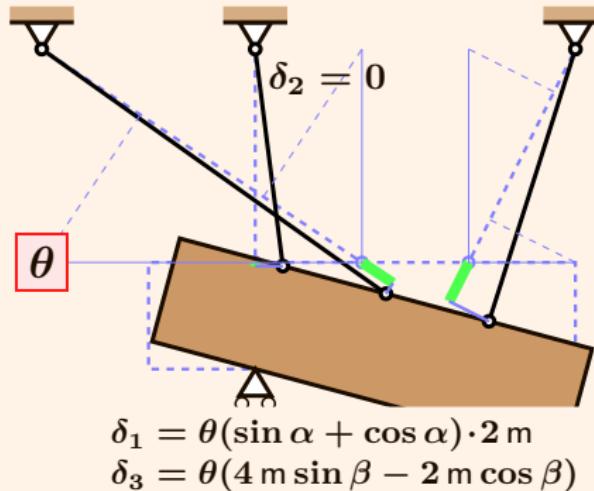
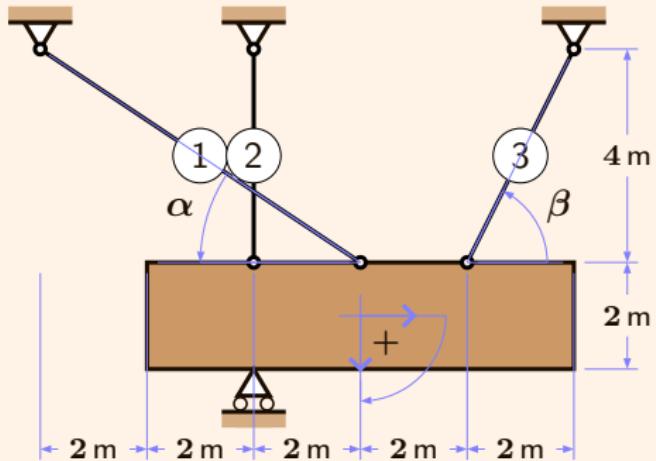
$$\delta_3 = -u \cos \alpha + v \sin \alpha + \theta \cdot 6 \text{ m} \cdot \sin \alpha$$

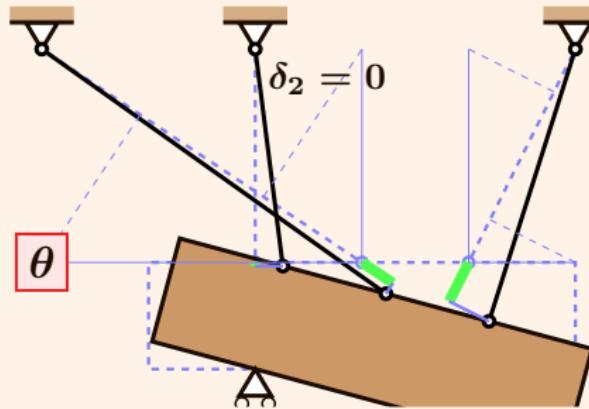
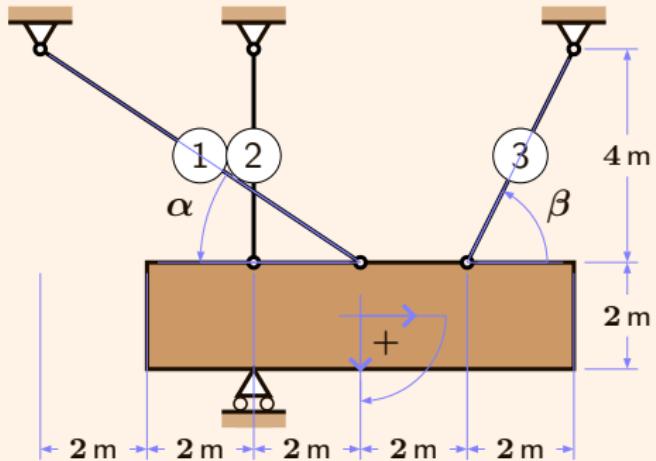






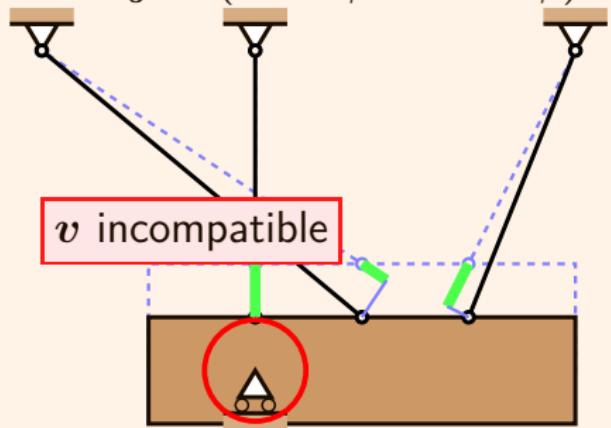
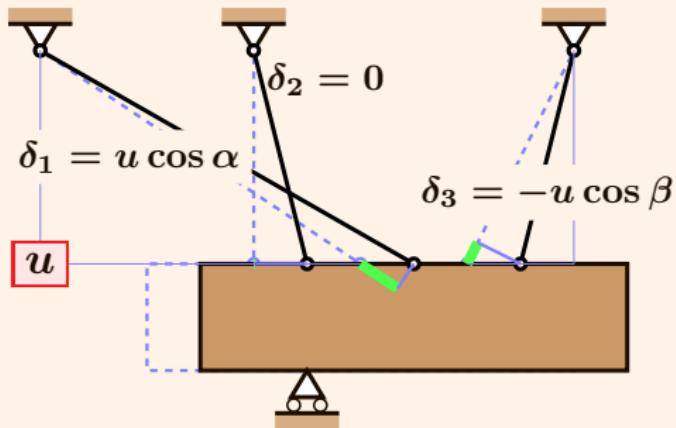


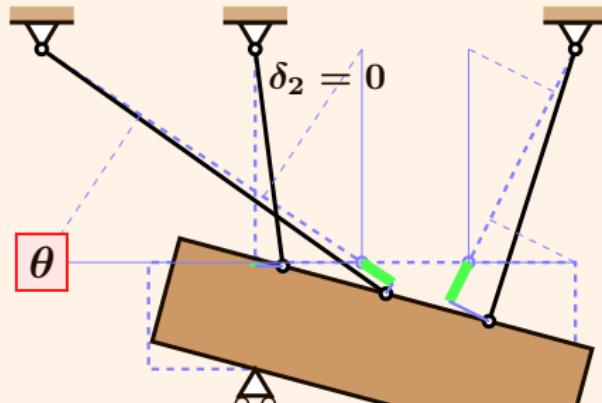
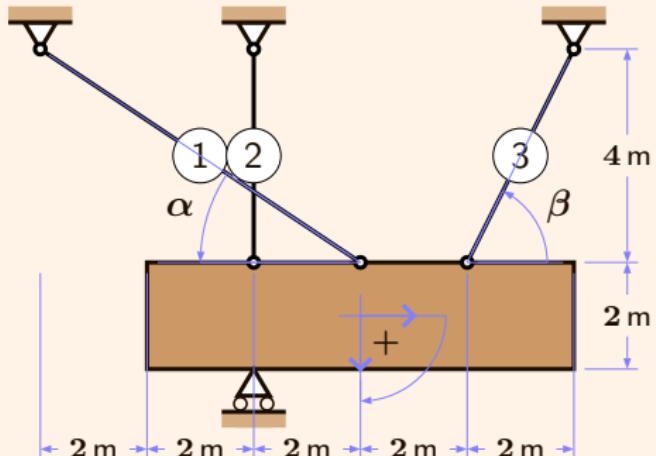




$$\delta_1 = \theta(\sin \alpha + \cos \alpha) \cdot 2 \text{ m}$$

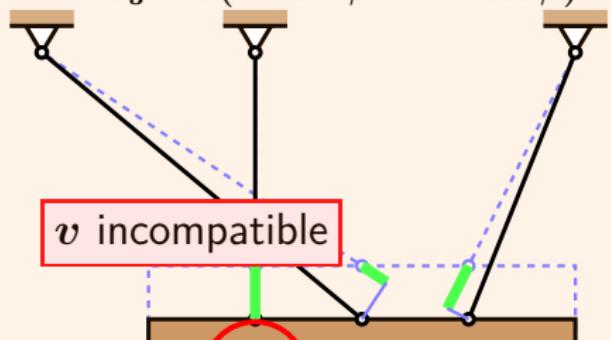
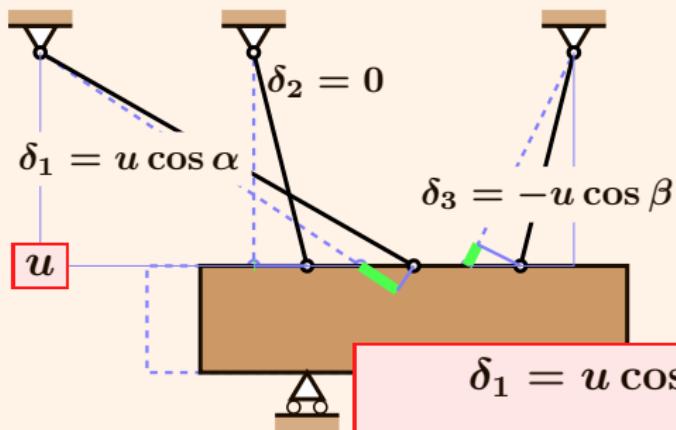
$$\delta_3 = \theta(4 \text{ m} \sin \beta - 2 \text{ m} \cos \beta)$$





$$\delta_1 = \theta(\sin \alpha + \cos \alpha) \cdot 2 \text{ m}$$

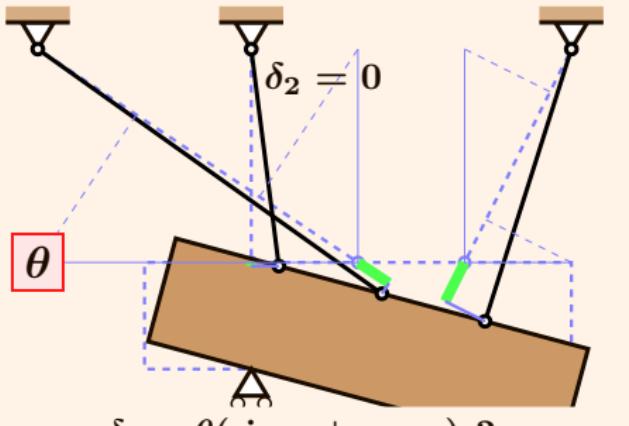
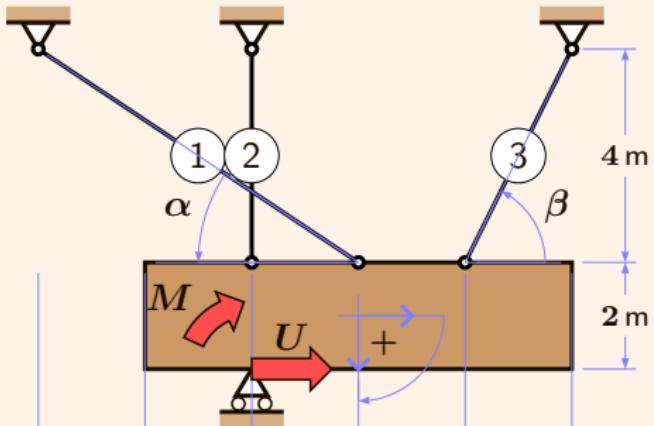
$$\delta_3 = \theta(4 \text{ m} \sin \beta - 2 \text{ m} \cos \beta)$$



**δ<sub>1</sub> = u cos α + θ(sin α + cos α) · 2 m**

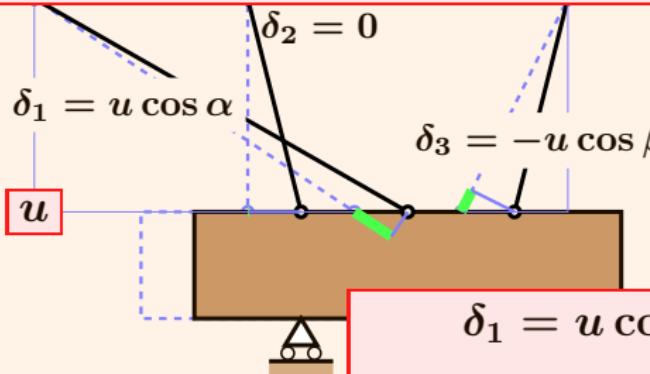
**δ<sub>2</sub> = 0**

**δ<sub>3</sub> = -u cos α + θ(sin β · 4 m - cos β · 2 m)**



$$U = N_1 \cos \alpha - N_3 \cos \alpha$$

$$M = N_1(\sin \alpha + \cos \alpha) \cdot 2 \text{ m} + N_3(\sin \beta \cdot 4 \text{ m} - \cos \beta \cdot 2 \text{ m})$$

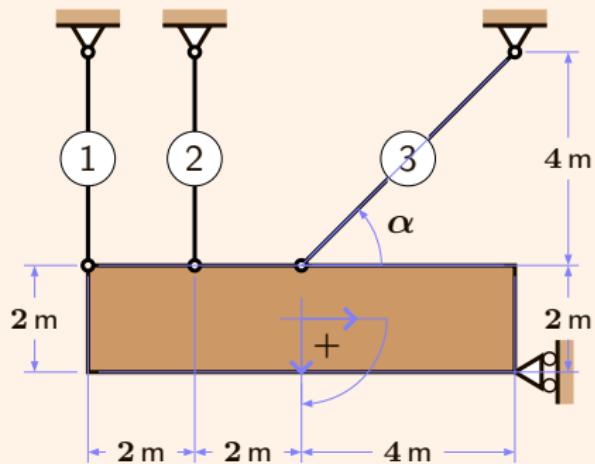


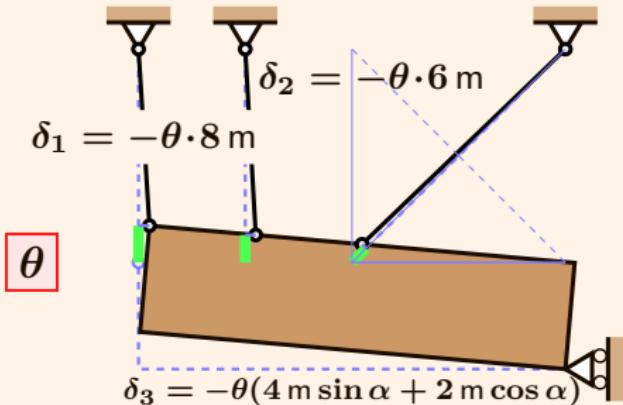
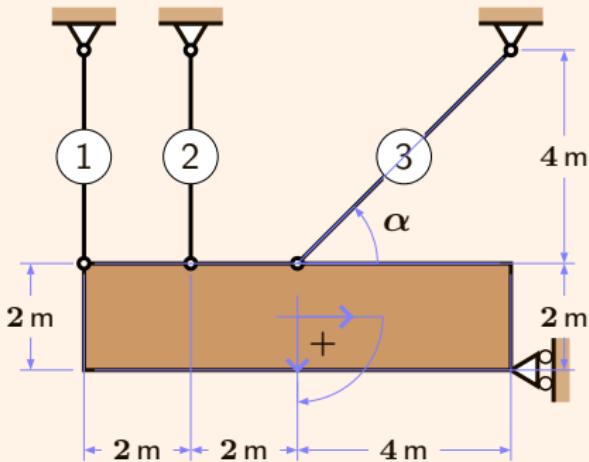
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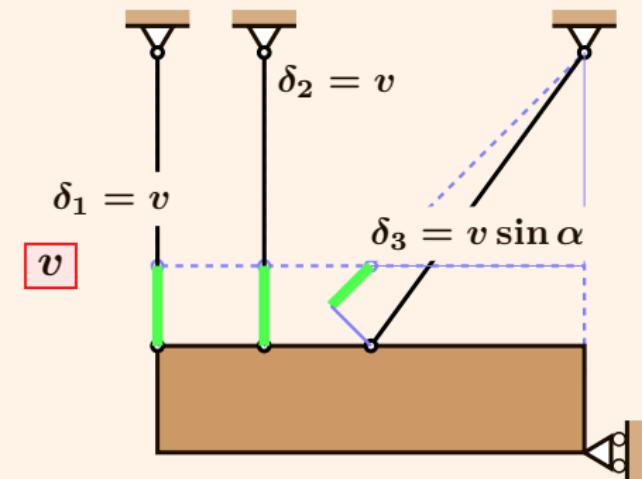
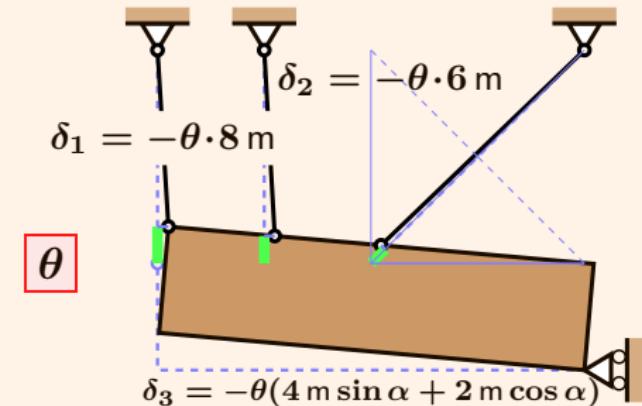
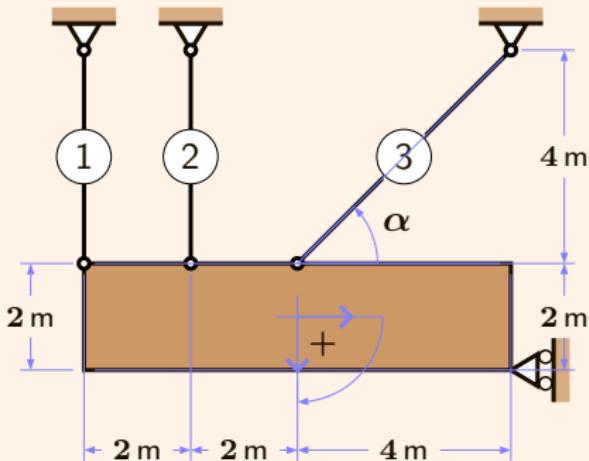
$$\delta_1 = u \cos \alpha + \theta(\sin \alpha + \cos \alpha) \cdot 2 \text{ m}$$

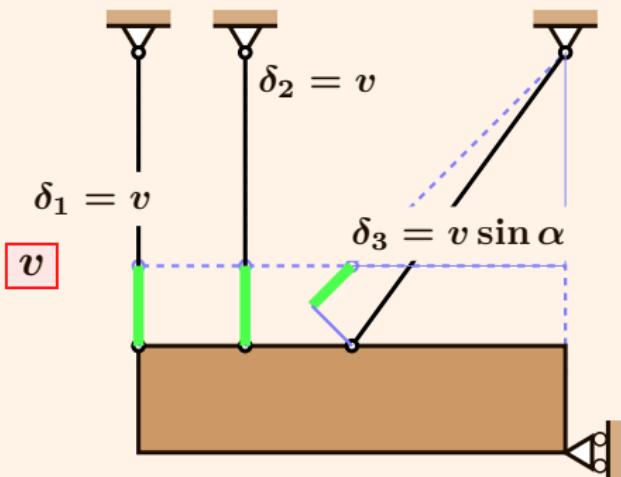
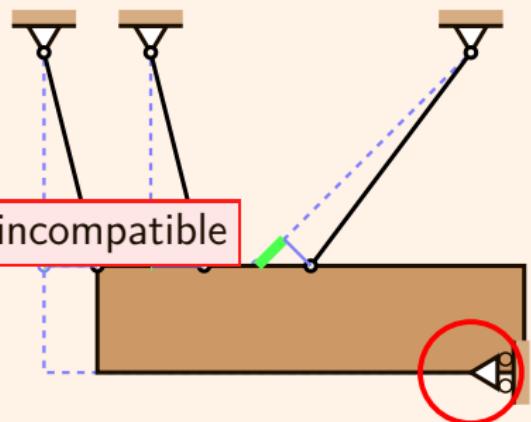
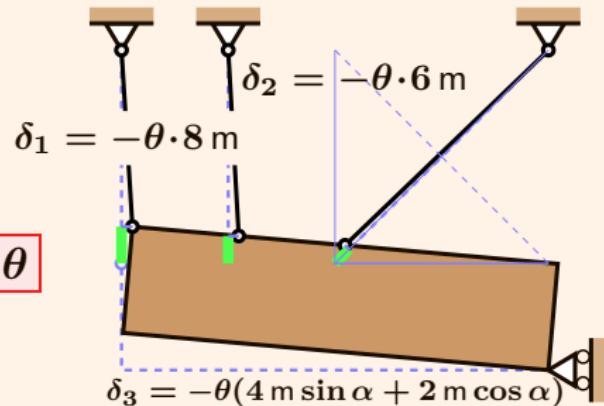
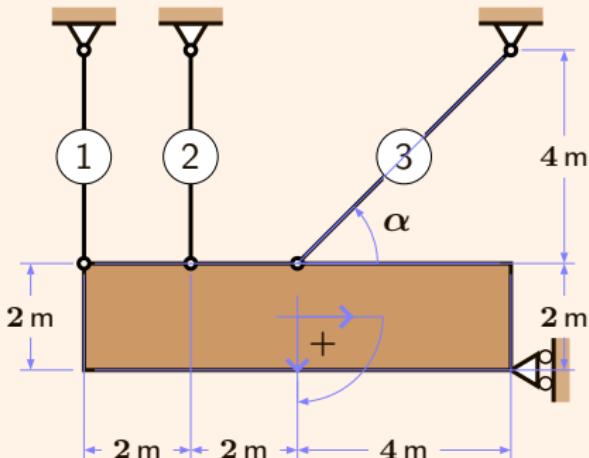
$$\delta_2 = 0$$

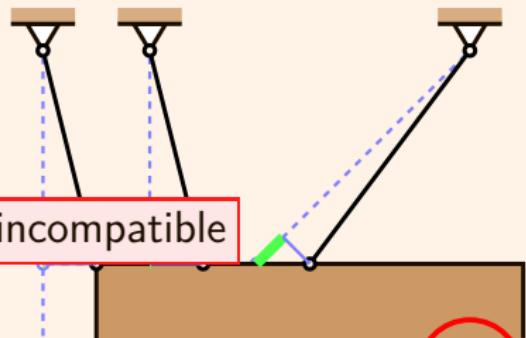
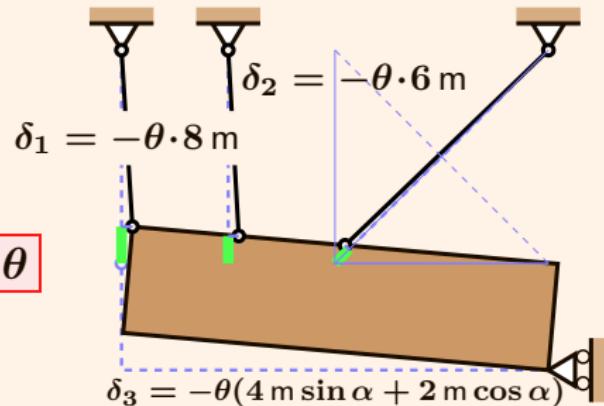
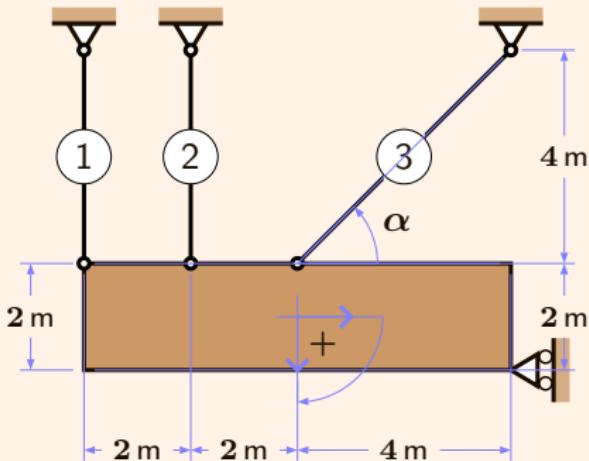
$$\delta_3 = -u \cos \alpha + \theta(\sin \beta \cdot 4 \text{ m} - \cos \beta \cdot 2 \text{ m})$$









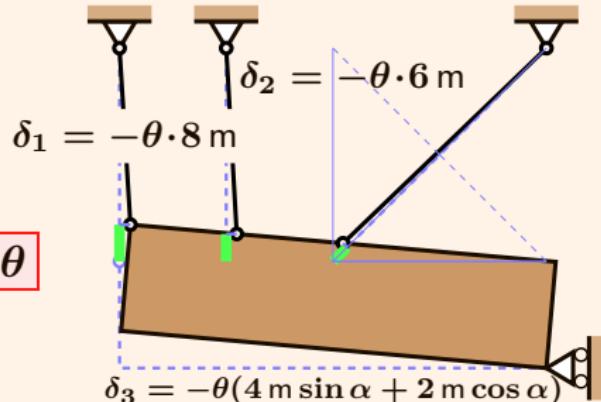
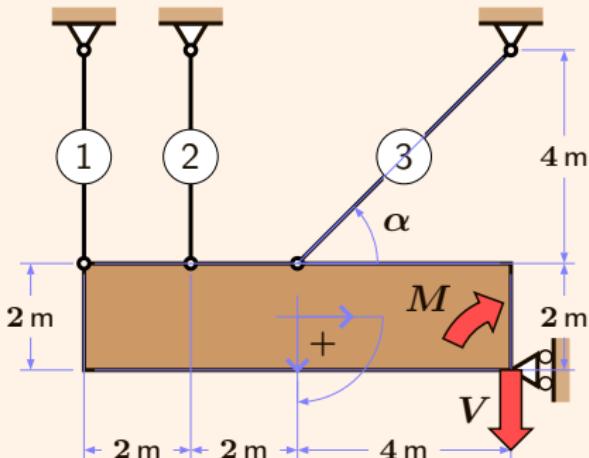


**$u$  incompatible**

$$\delta_1 = v - \theta \cdot 8 \text{ m}$$

$$\delta_2 = v - \theta \cdot 6 \text{ m}$$

$$\delta_3 = v \sin \alpha - \theta(\sin \alpha \cdot 4 \text{ m} + \cos \alpha \cdot 2 \text{ m})$$



$$V = N_1 + N_2 + N_3 \sin \alpha$$

$$M = -N_1 \cdot 8 \text{ m} - N_2 \cdot 6 \text{ m} - N_3 (\sin \alpha \cdot 4 \text{ m} + \cos \alpha \cdot 2 \text{ m})$$

**$u$  incompatible**

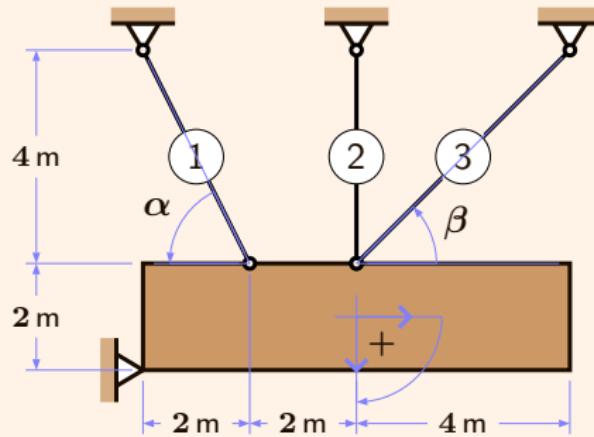
$$\delta_1 = v$$

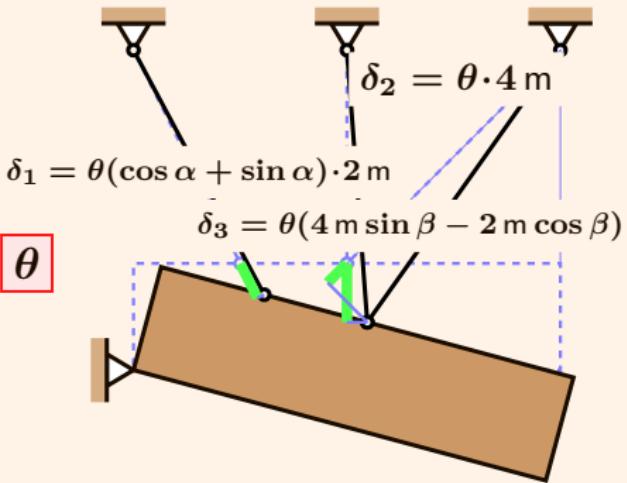
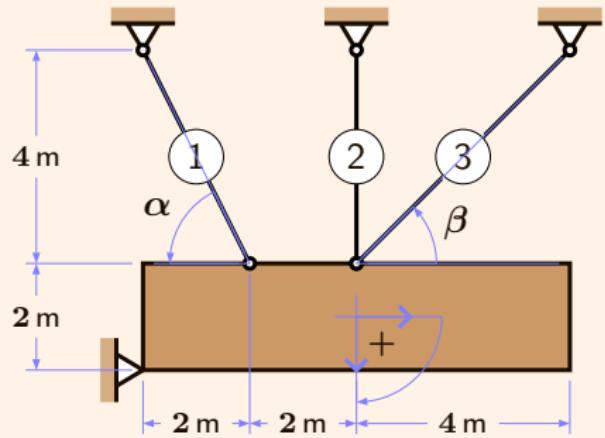
$$\delta_3 = v \sin \alpha$$

$$\delta_1 = v - \theta \cdot 8 \text{ m}$$

$$\delta_2 = v - \theta \cdot 6 \text{ m}$$

$$\delta_3 = v \sin \alpha - \theta (\sin \alpha \cdot 4 \text{ m} + \cos \alpha \cdot 2 \text{ m})$$





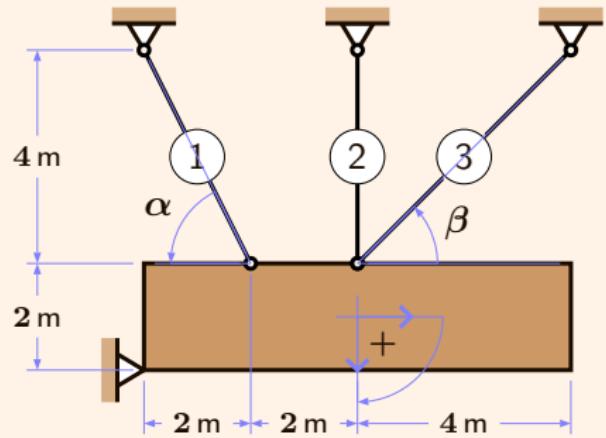
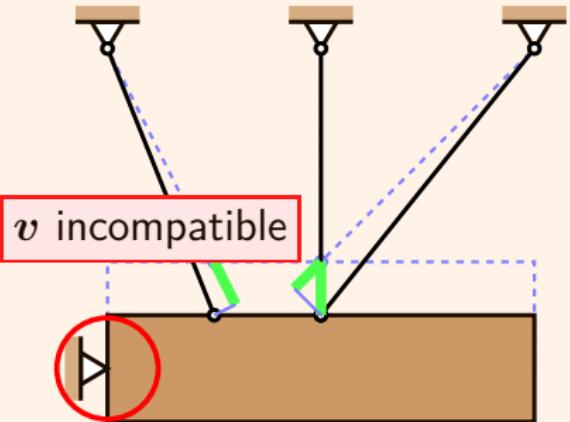
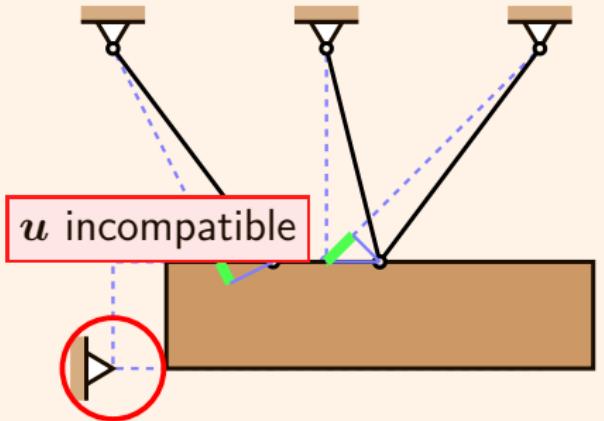
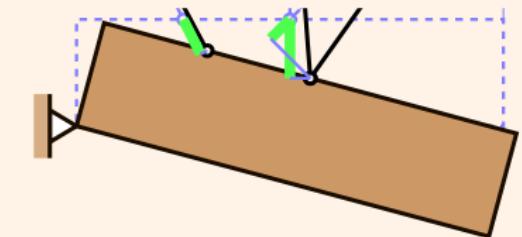


Diagram showing the beam deflected by an angle  $\theta$ . The deflection angles at the supports are  $\delta_1 = \theta(\cos \alpha + \sin \alpha) \cdot 2 \text{ m}$  and  $\delta_2 = \theta \cdot 4 \text{ m}$ . The deflection at node 3 is  $\delta_3 = \theta(4 \text{ m} \sin \beta - 2 \text{ m} \cos \beta)$ .



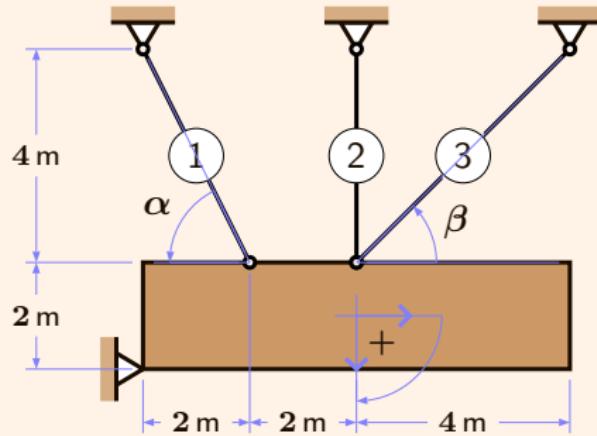
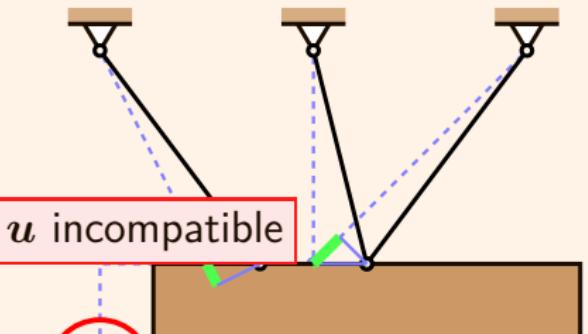


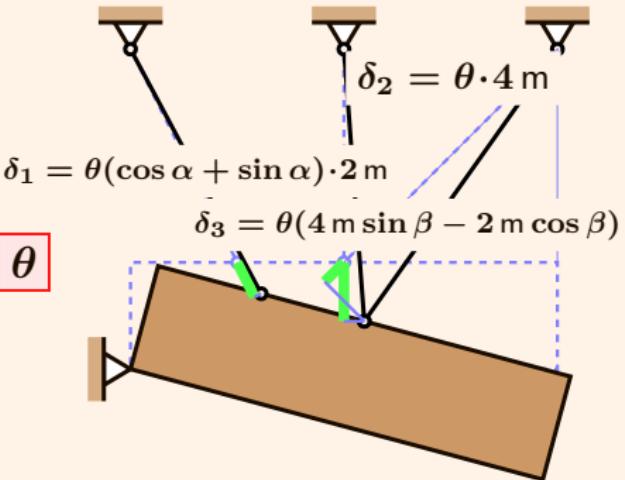
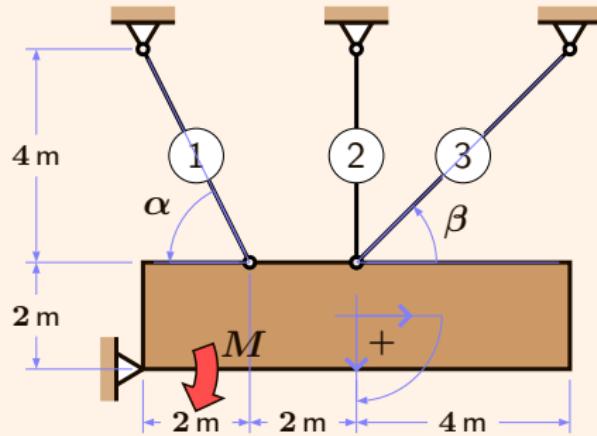
Diagram showing the rigid frame rotated by an angle  $\theta$ . The horizontal distance between the centers of nodes 1 and 2 is now  $\delta_1 = \theta(\cos \alpha + \sin \alpha) \cdot 2 \text{ m}$ . The horizontal distance between the centers of nodes 2 and 3 is now  $\delta_2 = \theta \cdot 4 \text{ m}$ . The vertical distance between node 1 and node 2 is now  $\delta_3 = \theta(4 \text{ m} \sin \beta - 2 \text{ m} \cos \beta)$ .



$$\delta_1 = \theta(\sin \alpha + \cos \alpha) \cdot 2 \text{ m}$$

$$\delta_2 = \theta \cdot 4 \text{ m}$$

$$\delta_3 = \theta(\sin \beta \cdot 4 \text{ m} - \cos \beta \cdot 2 \text{ m})$$



$$M = N_1 \theta (\sin \alpha + \cos \alpha) \cdot 2 \text{ m} + N_2 \cdot 4 \text{ m} + N_3 (\sin \beta \cdot 4 \text{ m} - \cos \beta \cdot 2 \text{ m})$$

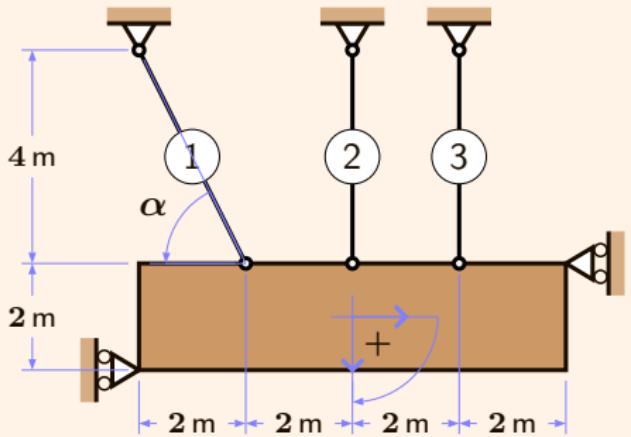
***u* incompatible**

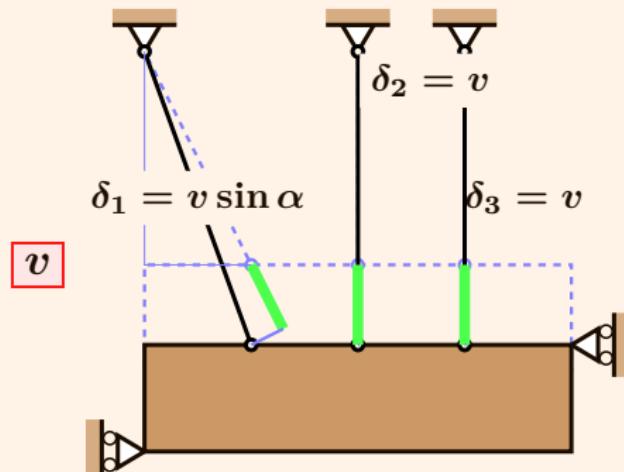
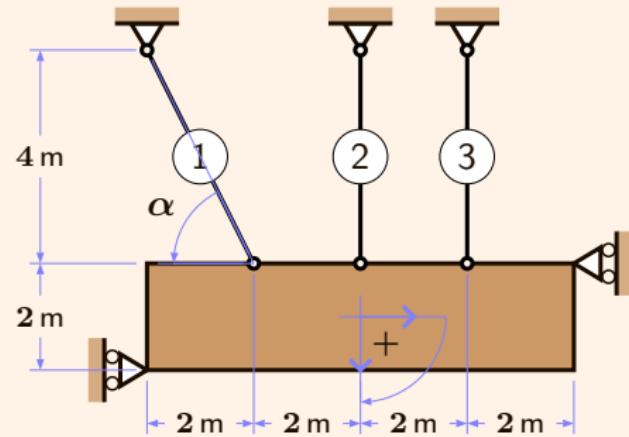
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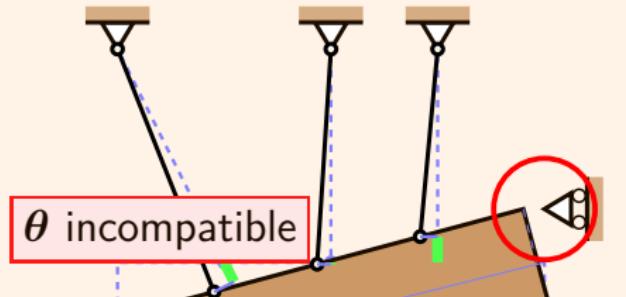
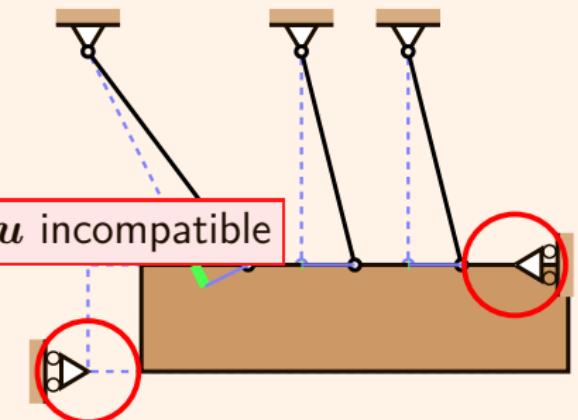
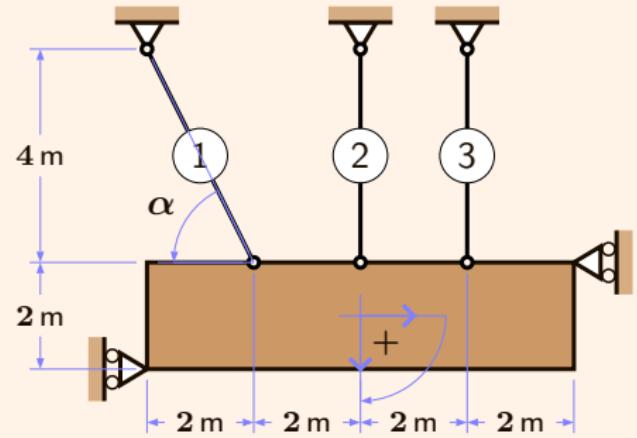
$$\delta_1 = \theta (\sin \alpha + \cos \alpha) \cdot 2 \text{ m}$$

$$\delta_2 = \theta \cdot 4 \text{ m}$$

$$\delta_3 = \theta (\sin \beta \cdot 4 \text{ m} - \cos \beta \cdot 2 \text{ m})$$



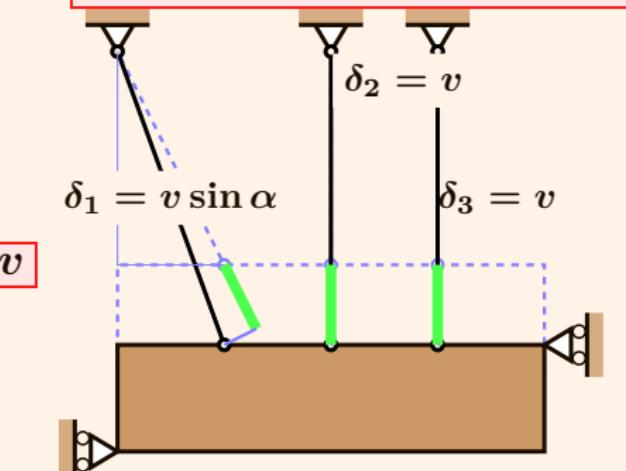


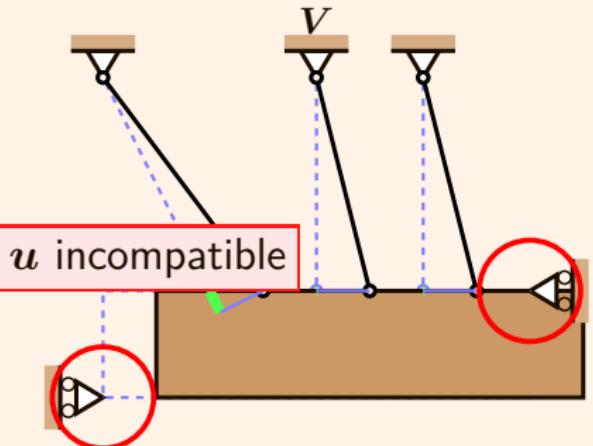
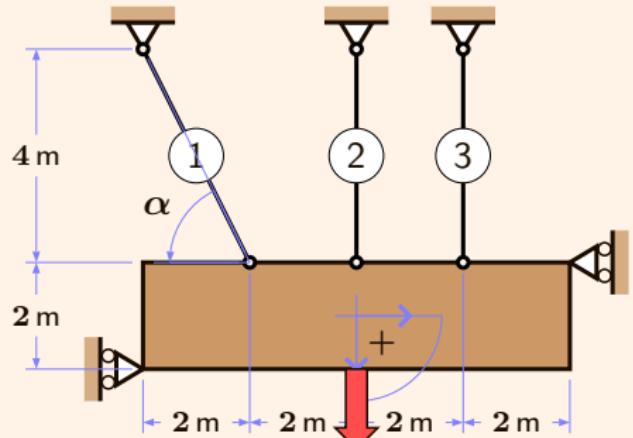


$$\delta_1 = v \sin \alpha$$

$$\delta_2 = v$$

$$\delta_3 = v$$

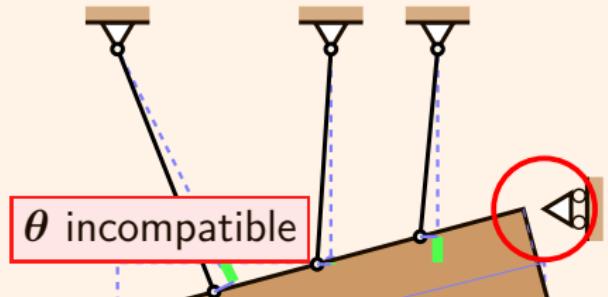




$$V = N_1 \sin \alpha + N_2 + N_3$$

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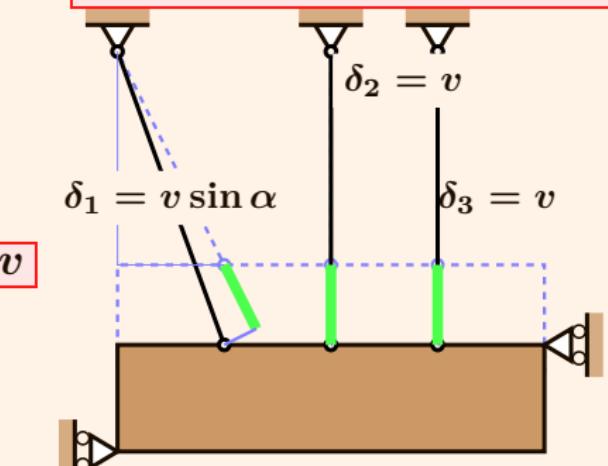
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$$\delta_1 = v \sin \alpha$$

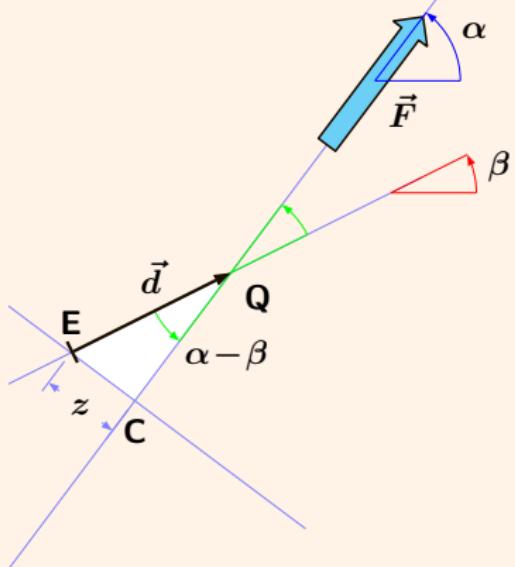
$$\delta_2 = v$$

$$\delta_3 = v$$



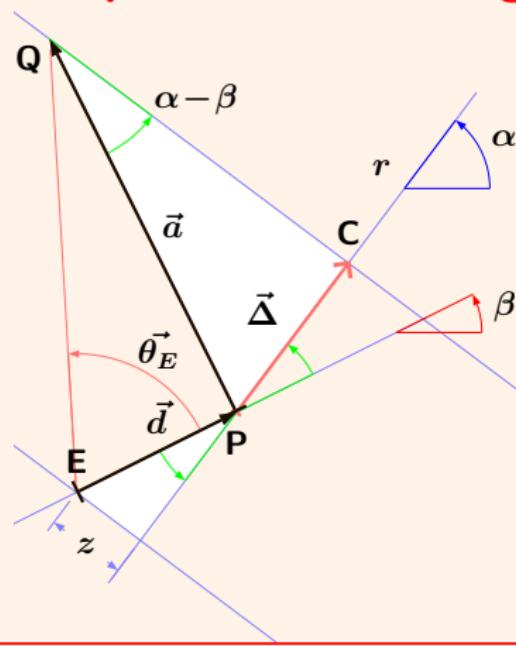
# Relaciones mecánicas y cinemáticas

## Momento de una fuerza



$$\vec{M}_E(\vec{F}) = \vec{F} \times \vec{d}$$
$$M_E = F \cdot d \cdot \sin(\alpha - \beta)$$
$$M_E = F \cdot z$$

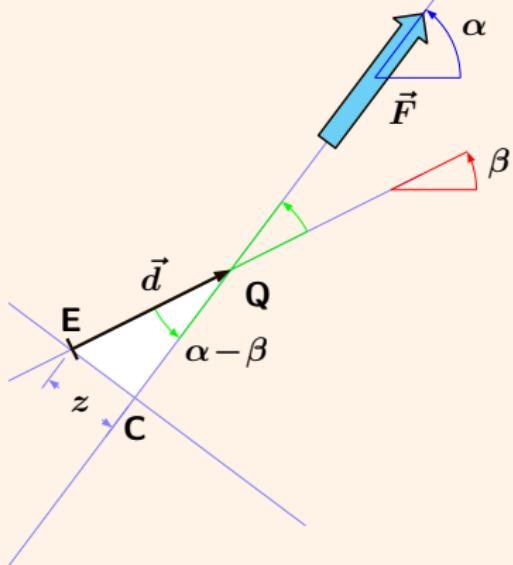
## Desplazamiento de un giro



$$\vec{a}(\theta_E) = \vec{d} \times \vec{\theta}_E; a = \theta_E \cdot d$$
$$\Delta = \theta_E \cdot d \cdot \sin(\alpha - \beta)$$
$$\Delta = \theta_E \cdot z$$

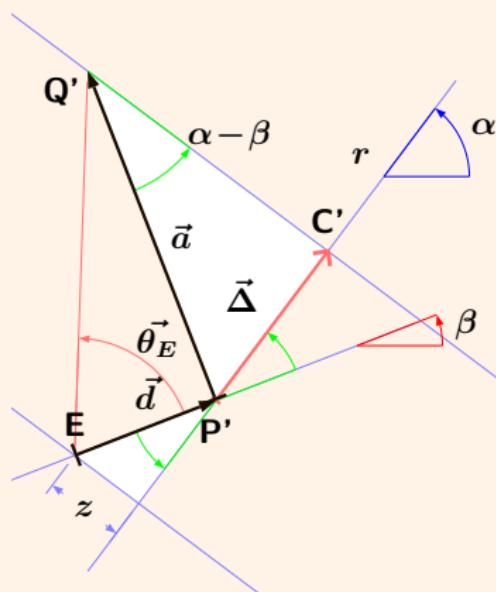
# Relaciones mecánicas y cinemáticas

## Momento de una fuerza



$$\begin{aligned}\vec{M}_E(\vec{F}) &= \vec{F} \times \vec{d} \\ M_E &= F \cdot d \cdot \sin(\alpha - \beta) \\ M_E &= F \cdot z\end{aligned}$$

## Desplazamiento de un giro



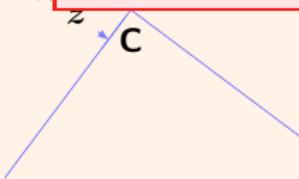
$$\begin{aligned}\vec{a}(\vec{\theta}_E) &= \vec{d} \times \vec{\theta}_E; a &= \theta_E \cdot d \\ \Delta &= \theta_E \cdot d \cdot \sin(\alpha - \beta) \\ \Delta &= \theta_E \cdot z; \vec{\Delta} &= \vec{z} \times \vec{\theta}_E\end{aligned}$$

## Relaciones mecánicas y cinemáticas

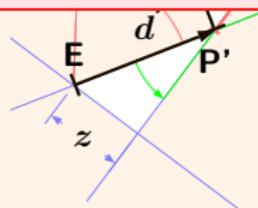
M La relación de “contravarianza” entre la pareja momento y giro y la pareja fuerza y desplazamiento, surge de la necesidad de que el trabajo de una fuerza resulte igual al trabajo de “su” momento:

$$\text{trabajo} = M_E \cdot \theta_E = (\mathbf{F} \cdot z) \cdot \theta_E = \mathbf{F} \cdot (z \cdot \theta_E) = \mathbf{F} \cdot \Delta$$

es decir, de la primera ley de la termodinámica, la de conservación de la energía.



$$\vec{M}_E(\vec{F}) = \vec{F} \times \vec{d}$$
$$M_E = F \cdot d \cdot \sin(\alpha - \beta)$$
$$M_E = F \cdot z$$



$$\vec{a}(\theta_E) = \vec{d} \times \vec{\theta}_E; a = \theta_E \cdot d$$
$$\Delta = \theta_E \cdot d \cdot \sin(\alpha - \beta)$$
$$\Delta = \theta_E \cdot z; \vec{\Delta} = \vec{z} \times \vec{\theta}_E$$

# Sólido deformable: compatibilidad y equilibrio (3rd ed)

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Universidad Politécnica de Madrid

<http://habitat.aq.upm.es/gi>

Edicion del 15 de marzo de 2017

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